The Health Care Center

Dauphin County, PA



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Construction Management Senior Thesis – Spring 2007 Dr. David Riley

Health Care Center Central Pennsylvania

Construction Management Ken Lorenz

PROJECT TEAM:

- **Owner:** Anonymous
- **CM**: Gilbane Building Co.
- Architect: Murray Associates
- **Structural Engineer:** Whitney, Bailey, Cox, Magnani
- MEP Engineer: Barton Associates
- Civil Engineer: Pennoni Associates, Inc.

STRUCTURE

- 4" Slab and slab-on-deck
- Cast-in-place continuous footing around the perimeter of building
- Structural Steel Columns on top of cast-in-place spread footings
- Structural Steel beams and girders connecting to the columns

ARCHITECTURE

• Facade consists of brick veneer and aluminum siding with aluminum clad windows to match the Art Deco style of the existing building

MECHANICAL, ELECTRICAL, & LIGHTING

- 10 Air Handling Units (3 in basement, 7 on roof)
- 500 kVA and 150kVA, 120/208V, 3 phase dry type transformers in basement
- Two 30kVA, 120/208, 3 phase dry type transformers in penthouse level
- Flourescent, Incandescent, and HID lighting throughout building

PROJECT FEATURES

- Occupation: Medical/Health Care Facility
- Construction Dates: August 06 -August 08
- Cost: \$25 Million
- Size: 100,000 SF
- Number of Stories: 2
- Leed Certified

CONSTRUCTION

- 20% renovation work and 80% new construction
- Existing building demolition requires removal of asbestos and lead paint
- Maintain use of existing building until renovation work completed



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EXECUTIVE SUMMARY

The following Spring 2007 Senior Thesis, for Penn State's Architectural Engineering program, will cover an entire school year's work and analysis on the Health Care Center, located in Dauphin County, Pennsylvania. Included in this report is a building overview, local conditions, building systems, proposal, research analysis, structural breadth analysis, mechanical breadth analysis, and recommendations to those analyses.

The building overview will give a brief introduction about the Health Care Center, the function of the building, project team involved and a brief introduction into the report. The local conditions will describe where the building is located and what the subsurface conditions are like. The building systems section discusses the structural, mechanical, and electrical systems along with other interesting facts about the building.

The proposal will briefly describe what will be analyzed in the research and breadth topics. The research topic will be analyzing the integration of value engineering and sustainability; a topic that affects the construction industry. The purpose is to incorporate value engineering to a project that is striving for LEED or another sustainable status. Value engineering will be used to find alternative solutions without affecting the building's green accreditation. The structural breadth will analyze a six inch concrete foundation wall that extends sixteen feet high to the roof elevation. The mechanical breadth will examine the Health Care Center's plumbing system, finding an alternate system to the increasing problem of highly priced copper piping.

After the analyses, a recommendation is made on the two breadth areas that will be most beneficial to the Health Care Center.

ACKNOWLEDGEMENTS

I would like to thank all of the people and companies that have helped me throughout my thesis research. First and foremost I would like to thank the anonymous boarding school and their Planning, Designing and Construction division who allowed me to use the Health Care Center and all the areas of research. Without them I would not have been able to use their building. Next I want to thank Gilbane Building Company, especially Dennis Vance and Lee Sokloski, who thought of the project and directed me to Andrew Notarfrancesco, the project manager. Andrew, thank you for answering all of my questions and supplying me with all of the drawings. I also want to thank the rest of the project team that is working on the Health Care Center. A special thanks to Terry Saad from Whitney, Bailey, Cox & Magnani for helping me with my structural analysis. Thank you to everyone in the construction industry who responded to my emails and questions. Also, thank you to all the Penn State Architectural Engineering faculty and staff, especially the construction management professors. Lastly, I would like to thank all of my family and friends for their support and help.

BUILDING OVERVIEW

INTRODUCTION

The Health Care Center, located in Dauphin County, Pennsylvania, is an addition and renovation project that will be serving a boarding school, who wishes to remain anonymous, as well as its local community. The Health Care Center's function is similar to medical facilities found on college campuses, such as the Ritenour building on Penn State's campus, which serves as an infirmary, workplace, and educational tool. The building's addition will include new rooms for patient care, office and administrative space, a cafeteria and kitchen, and a gymnasium. The work involved in this project will be extensive and costly and will need to incorporate an integrated team to deliver and meet expectations.

The project team involved in this process is the boarding school's own Planning, Designing, and Construction division, Murray Associates (architect), Whiney, Bailey, Cox, & Magnani (structural engineers), and Gilbane Building Co. (construction managers). The Health Care Center is a partial two story above grade structure with a partial basement level. The project, which will be going for LEED (Leadership in Energy and Environmental Design) certification, will be 80,000 square feet (SF) of new construction and 20,000 SF of renovation. The project delivery method chosen for the Health Care Center is design-bid-built with Gilbane contracted as a CM agent. The total duration of construction was scheduled for a full 2 years beginning in August 2006 and completing in August 2008. Due to some unexpected set-backs mentioned later in the research, the project has been delayed. The overall cost of the project is expected to reach \$25 million. The intricate details of the Health Care Center's renovations and additions will be described throughout the thesis.

The following analysis will focus on the construction management aspect of the Health Care Center with special considerations in constructability, cost impact and schedule reduction. The integration between value engineering and sustainability will be analyzed and studied to help the construction industry. The integration between the two will also be used in areas of the Health Care Center where the building can save some money while still maintain its LEED certification. These areas specifically refer to the redesign of a foundation wall and an alternative use of a cross-linked polyethylene tubing, called PEX, which will replace the existing domestic water supply's copper piping. Please note that all information pertaining to the Health Care Center is Ken Lorenz's interpretation and may be different than the means and methods of construction executed by the project team.

LOCAL CONDITIONS

CLIENT

The Health Care Center is operated and owned by an anonymous boarding school that was originally founded in 1909. It started as an idea from a wealthy and successful businessman and his wife who lived in the area, to help children who were less fortunate. Since then the school grew to over 1400 students. With the increase in the student body, the existing Heath Care Center needed more room to accommodate and provide even more care for their students. The owner is very experienced in construction and the additions are one of many buildings that have expanded the boarding school.

LOCATION

The location of the Health Care Center is in Dauphin County, which is located central Pennsylvania (see Figure 1). In this particular area of Pennsylvania, structural steel framing with slab-on-deck buildings seems to be the most common method of construction. Steel buildings are typically less costly and can be erected faster than concrete buildings.



Figure 1 - Picture of Pennsylvania's counties.

SUBSURFACE CONDITIONS

The Health Care Center falls in the Valley and Ridge Physiographic Province which is predominantly made up of bedrock and limestone. Topsoil and bituminous pavement cover large parts of the construction site. Sieve and hydrometer tests were taken to determine that subsurface soil conditions also consist of sands, silts, clay, and mixtures of all of them. Based on all the information from the tests, the soils were concluded to be suitable for the proposed construction. The water table was measured at an elevation height of 380, which is 20' below the existing ground surface elevation. Since the basement elevation will be positioned at 391.7 the water table should not impact the construction of the building. The contour of the Heath Care Center site tends to slope downward in a south to southwest direction in which gradients range from 2 to 3 percent in some areas to 6 to 8 percent in other areas.



Figure 2 - The valley and ridge physiographic province.

BUILDING SYSTEMS

DEMOLITION

The Health Care Center is 80% new construction and 20% renovation work which makes up the 100,000 SF of total construction. Because the original structure was erected in the 1930's, hazardous materials were used in the original design and must be removed before any construction/renovation can take place. A special demolition contractor has to remove the hazardous materials which include asbestos and lead paint during the renovation work of the existing building. All existing HVAC and lighting, including wiring, fixtures, raceways, light switches, and receptacles are to be removed from the existing building. Before renovation work can begin all new additions must be completed. This is because the Health Care Center must remain operational during the construction process.

STRUCTURAL

The frame of the Health Care Center is a typical structural steel frame. Each steel column is erected on top of cast-in-place concrete spread footings. Cast-in-place concrete foundation walls will be poured in sections B and C (sections shown in Appendix A). Sections A and B will include the basements of the newly remodeled/constructed building. The rest of the buildings perimeter will have a 3 foot deep continuous footing. Building sections C through E will have a 4" concrete slab-on-grade. All cast-in-place concrete will use both horizontal and vertical formwork. Most of the building's framing is made up by wide flanges with metal decking and a 4"slab-on-deck. The roofing uses wide flanges in some areas and steel joists in other areas, like the gymnasium.

MECHANICAL

The mechanical system is very important for the Health Care Center. A section of the Health Care Center will be used as an infirmary which means the air must be free of germs and bacteria that are likely to spread if a good ventilation system is not in place.

The building must also maintain good, indoor air quality for the building to be LEED certified.

There are a total of ten air-handling-units throughout the Health Care Center. There are three located in the basement while the other seven are on the roof. The three in the basement will serve the existing building and cafeteria area, while the other seven will be utilized by the gymnasium, the penthouse, and other new additions. Throughout the building there are exhaust fans, variable air volume (VAV) boxes, cooling towers, and humidifiers. An Electric Control System will be in place to operate and monitor the air system to ensure the air quality stays at healthy and LEED certified levels.

ELECTRICAL/LIGHTING

The Health Care Center's electrical system is composed up of a 500 KVA, 150 KVA and two 30 KVA dry transformers. The 500 and 150 KVA transformers are located in the basement of the building. These transformers are converting the electricity down to 120/208 V and distributing the power to panel boards located on the first and second floors.

The two, smaller 30 KVA transformers are located in the penthouse area where they will convert the electricity to 120/208V. After converting the electricity, the power will be distributed to panel boards throughout the penthouse. As in many other commercial buildings, a majority of the Health Care Center's lighting fixtures are fluorescent. However, in some areas of the building, incandescent and metal halide fixtures are also used.

MASONRY / FAÇADE

The buildings façade consists mostly of brick veneer with aluminum clad windows. The brick is not load-bearing; it only needs to support its self weight. A few parts of the building, like the penthouse, have aluminum siding. The cafeteria has a curtain wall, where there are large aluminum clad windows looking into the dining room.

PROPOSAL

This proposed senior thesis study of the Health Care Center, located in Dauphin County, PA, will concentrate on the research of integrating value engineering (VE) and sustainability. The main idea of this research is to focus on a building that has been designed for LEED or other environmental/energy saving criteria to go through the VE process and not loose any of its sustainable accreditation.

After conducting research on sustainability and value engineering (Research Topic), the Health Care Center will be analyzed in two areas (Structural and Mechanical Breadths) where VE can be utilized to reduce costs, increase productivity, and ensure quality without diminishing the sustainability of the building.

RESEARCH TOPIC – Value Engineering and Sustainability

- Value Engineering and sustainability will be researched so that when executed on any one particular project, green ideas and materials will not be eliminated.
- Areas that will be examined will be the following;
 - What is value engineering?
 - What is involved to ensure a productive value engineering process?
 - Sustainable considerations that should be looked into during the conceptual planning, designing, and construction phases.

STRUCTURAL BREADTH – Redesign of Concrete Foundation Wall

- Alternative Design foundation wall out of CMU block.
 - Proposed Benefit Lower material and labor cost, possible schedule reduction while maintaining thermal insulation of wall.

MECHANICAL BREADTH – PEX Tubing for Domestic Water Supply

- Alternative Replace the domestic water supply copper tubing with PEX tubing.
 - Proposed Benefit Lower material and labor cost, and possible schedule reduction while adding sustainable design to project.

RESEARCH TOPIC

Value Engineering and Sustainability

PROBLEM

In today's world there is an increasing interest in making things environmentally friendly. The construction industry has gone into green thinking by adopting LEED (Leadership in Energy and Environmental Design) as one of their criterion to determine whether a building is sustainable. Unfortunately, green buildings tend to be a bit more expensive to design and construct than a non-green building. Green materials or products may be more expensive and labor costs may be driven higher because contractors are unfamiliar with that type of work. Not only does a green building affect the cost, but it also impacts the schedule. Special commissioning may need to take place for MEP systems, lead time may be needed for green materials that have to be shipped in, and construction can take longer for laborers who are inexperienced with the type of work.

The research that I will be investigating not only pertains to the construction industry as a whole but also to the Health Care Center. As stated earlier, the Health Care Center is striving for LEED certification and over the last few months, the project has been going through the VE process due to bids coming back over budget.

GOALS

Through my proposed research I hope to develop an approach that effectively and efficiently uses value engineering on any construction project with the outcome of maintaining or even gaining sustainability. I also hope that the construction industry can get a better understanding of how to use value engineering as a tool without reducing a building's sustainability. Lastly, I will be taking the information found from my research and applying it to the Health Care Center. I will be looking into two areas, structural and mechanical, where alternative systems will be evaluated on terms of costs, schedule, quality, and sustainability.

I will use all resources available to come up with the most important and relevant information for my research. I will begin with researching and understanding the methodology of VE. Much of this information can be found in class notes, books, and online. SAVE International (Society of American Value Engineers), which is the international society devoted to the advancement and promotion of the value methodology, will be very beneficial for value engineering ideas and methods. For more information, I will contact industry professionals who are familiar with this area. Next, I will make myself familiar to the LEED manual and research sustainable ideas.

I am confident that through researching and becoming familiar with VE and green ideas that I can develop an effective method to ensure that VE, if used correctly, can reduce project costs without loosing sustainability requirements and status. I will combine the energy saving/environmentally friendly ideas with good VE practice and methodology to make a successful integration between the two. Lastly, after developing a VE and sustainable practice, I will use it for breadth topics for the Health Care Center, which will be discussed later in this report.

ANALYSIS

Introduction

There are a few misconceptions when it comes to value engineering (VE). What is value engineering exactly and what is involved in the value engineering process? Value engineering is not cutting costs, but rather "a systematic effort to find less costly ways to meet the Owner's needs in the building without sacrificing the scope, quality, aesthetics, operating costs or long term maintenance and replacement costs." Applying VE to a sustainable building means that the environment, energy consumption and overall health of the occupants will be taken into consideration when the most value alternative is chosen.

The Value Engineering Process

The value engineering process involves information gathering, analysis, creative brainstorming, evaluation, recommendation, and lastly implementation. It is important to understand the VE process when evaluating a building's alternatives. This will be even more costly when trying to find an alternative solution that requires maintaining the buildings environmental requirements.

Information Gathering

This part of the process, a team wants to learn and gather as much information about the project as possible. Learn what the goals are from the owner, what type of quality needs to be met, what types of building systems are being used, what the budget is, what is the proposed duration of the project, and any other important information. Everything gathered will be used in the next step.

Analysis

In this next step, all the information that was gathered in the first step will be analyzed. Thoughts on why certain systems and materials chosen will come into play. Are there possible alternatives to everything that is included in the current proposed building? Many questions should arise to determine why certain objectives were chosen.

Creative Brainstorming

This part of the process is essentially where the alternative solution comes from. Every innovative and creative possible solution should be thrown out as an idea. There is no wrong idea. The main focus during this part of value engineering is to develop as many possible solutions, so they can be evaluated in the next step to see if feasible.

Evaluation

The most innovative and best ideas developed from the creative stage will now be evaluated. They will be examined closely in cost, quality, duration, and energy savings. This stage will determine the most feasible and beneficial solutions.

Recommendation

Once the alternative solutions have been picked, the VE team will propose the new ideas to the project team and owner. Here the project team along with the owner will determine what alternatives will be chosen, for the good of the building.

Implementation

The most important of the VE process, implementation involves making sure the ideas proposed and recommended are taking place. This part of the process will ensure that the new ideas are being incorporated into the building.

Value engineering, as described in the previous stages, is a process that should occur during the entire building process (see Figure 3 on the next page). It should begin very early and often in conceptual planning and continue through the design of the building, carry on through the construction, even during operation. Before ideas of sustainable alternatives should begin a few things must happen and carry out through the project. This includes building an integrated team, documenting/auditing all of the ideas and work performed, and performance strategies and implementation.



Figure 3 – The process of designing/constructing a building.

Integrated Team

It is important that at the beginning of any project the people involved sit down and form a team. The people who should generally be involved in these integrated teams include the owner, architect, engineers, construction manager, contractors, value engineers, and any other environmental /energy engineers. The first thing that should be done is to set a common goal. If individual parties are not enthusiastic or have different goals it will be harder for them to work together. This is also a good time to identify roles. Will the construction manager be acting as the value engineer or will there be a VE consultant? The only way that the team will be successful is if there is clear communication between individuals. This should be done by holding meetings every other week or in cases where a project is behind schedule or over budget, every week. At these meetings the team can:

- Establish sustainable objectives and make certain that these objects are being met.
- Make decisions about resources, materials, objectives, and short and long term building performances.
- Ensure that the contract documents are written to support sustainable design, construction and performance objectives.

Documentation and Auditing

Anything and everything should be well documented during each phase of the design and construction of a building. For one reason in particular, people may come and go, or there is a change of leadership on a project. Well documentation will help new people that are put on the job. They can get caught up in the project and become useful to the

project team immediately. Another reason would be that if something unfortunate happened and someone was sued. Document should also occur for staff turnover, project delays, and budget cuts.

Performance Evaluations

The significance of performance evaluations are to determine if the sustainable goals and objects that are set in the early stages of the design process are met. There has to be some sort of measurement to make sure that the goals are on progress and will finally be met. These measurements should be determined at the beginning when the objects and goals are first established. These evaluations may vary depending on the system or product. Evaluations are still useful even if the object is not met at the end of its proposed duration. They can be used as a lesson learned, and may be useful for future projects.

Value Engineering Integrated with Sustainability

As mentioned earlier, value engineering should be implemented as early as possible in the planning, designing, and construction process. The earlier VE is involved the more sustainable and life cycle costs can be evaluated which will have an impact on the design, construction, and operation of the building. Conceptual planning and the design/construction phase are areas where sustainability can be influenced the most through VE (see Figure 4 below).



Figure 4 - VE used during conceptual planning, design and construction.

Conceptual Planning Phase

During the conceptual planning phase is where decisions determine whether or not requirements developed in the first phase can be met by an addition, renovation, or new construction. Some things that are looked into and researched are whether a building could just suffice by having upgrades or should a brand new facility need to be built. This is also the time when VE can greatly influence sustainable ideas into the analysis. The following are areas where sustainability concentration should occur.



Figure 5 – VE during the conceptual planning phase.

Value

engineering

Site

- Determine whether the site chosen is suitable for new or additional construction.
- Choose an area that is already developed to minimize the development of open space.

Value

engineering

- Take advantage of the site's solar angle by positioning the building towards the sun.
- Integrate the building into the site's natural setting.

Energy

- Chose a site close to public transportation systems to reduce the use of fuel used by commuters.
- Use the site's natural characteristics to get the most out of the lighting, heating, cooling, and ventilation.
- Use technology to integrate the possibilities of solar and other alternative energy sources.

Materials

- Use local materials when ever possible.
- Avoid products that are non-renewable or non-reusable.
- Establish goals to maximize the use of environmentally preferred products in the buildings design.
- Review the life-cycle and first costs of materials and products.

Water

- Develop strategies for irrigation runoff.
- Use facilities that accommodate watershed drainage.
- Develop a rainwater catchment that can segregate the dirty water from potable water systems

Indoor Environment Quality

- Use natural ventilation.
- Establish lighting and acoustical criteria for design.
- Establish goals for using materials that minimize toxic emissions.
- Develop objectives to maximize daylight.

Operation & Maintenance

- Conduct continuous commissioning.
- Get information about indoor air quality and energy consumption from existing facilities.
- Ensure the delivery of a complete and thorough building operations manual.

Design Phase

Once the owner is confident they have sufficient funds to pay for the construction of a building, the designing phase begins. During this time the choice of materials, quality of design and construction, building layout, and types of systems will be explored. At this point and time of the process, VE can be used to analyze sustainable alternatives into the design of the building. The following are areas where sustainability concentration should occur.

Design Phase



Figure 6 – VE during the design phase.

Contract

- Determine what level of sustainability should be achieved (LEED certification?).
- Determine what contract methods will best support the achievement of sustainability.
- Determine what delivery method should be used.
- Determine what, if any, incentives should be included.
- Determine who will be the party enforcing sustainability.
- Determine what levels of commissioning should be required.

Site

- Choose the orientation of the building, taking advantage of the climatic features.
- Promote less automobile transportation by providing a pedestrian friendly setting and bicycle racks.

• Save all trees and shrubbery.

Energy

- Incorporate solar power into the design.
- Use shades and blinds for the summer and stone masonry for the winter.
- Plant trees to block the wind and provide shade.
- Enhance thermal properties by increasing wall mass.
- Use low-e and argon filled windows.

Materials

- Use demountable and reusable materials for interior components.
- Use low maintenance materials.
- Use locally available materials.
- Avoid materials that pollute and are toxic when manufactured.
- Use alternate materials.

Water

- Incorporate water conserving cooling towers.
- Use ultra low fixtures and waterless urinals.
- Eliminate lead-bearing products in potable water.
- Recover non-sewage water for on site use.

Indoor Environment Quality

- Provide thermal comfort with maximum personal control over temperature and humidity.
- Control dust and odors with proper ventilation.
- Comply with indoor air quality standards.
- Keep air intake ducts away from loading docks and driveways.
- Avoid materials that contain hazardous or toxic materials.

Operation & Maintenance

- Specify durable and low-maintenance materials and equipment.
- Position equipment for easy access for maintenance.
- Include the facility manager or building engineer on project team.

Construction Phase

The construction phase will begin when the scopes of work are developed during the design phase. The biggest challenge during the construction phase is managing changes that result from change in scope, errors and omissions in the plans and specifications, unforeseen conditions, and cost overruns. This is a point in time when VE is used to find alternatives to these problems. It is important that the building maintains its sustainability. The following are areas where sustainability concentration should occur.



Figure 7 – VE during the construction phase.

Site

- Preserve all trees and vegetation.
- Stock pile soils during excavation and redistribute later.
- Replant trees.
- Install a retention pond to prevent pollution of watershed.
- Have designated parking, storage, recycling, waste and cleaning areas.

Energy

- Conserve energy during construction operations.
- Have prefabricated materials shipped to site so systems can be assembled and installed easier.

Materials

- Incorporate a waste management plan including ideas for recycling and salvaging construction waste.
- Reuse concrete forms as much as possible.

• Ensure that green materials and products are being met by specifications.

Water

- Preserve the watershed from pollution by installing filtration barriers.
- Conserve and maintain the waste of water.

Indoor Environment Quality

- Flush out entire building of dust and dirt before deeming the building operational.
- Implement the commissioning plan to ensure proper operation and performance of all energy serving equipment.

Operation & Maintenance

- Conduct building commissioning to ensure all systems are working as specified.
- Make sure operations staff is familiar with procedures maintaining efficient performance.
- Provide a digital control system to maintain peak performance of systems.

CONCLUSION

There are many misconceptions about value engineering. It is not a quick and cheap way to cut costs, when a project is over budget. It is important to truly understand, what value engineering is and what is involved in the process. Value engineering can be a very effective tool when used, and when used properly it can maintain environmental and energy saving criterion.

When starting the VE process for a sustainable building, the one performing the value engineering should be well aware and understand the process involved. When gathering information, analyzing, creative brainstorming, and evaluating, the environment should be kept as a high priority.

Once the VE process is understood, an integrated team should begin to form to get the best results for the building. The better the team works together, the smoother the project will go. It is also critical to grasp the importance of documenting all of the ideas and work during the process. Performance evaluations and measurements should also be created to ensure that all sustainable objectives are being met.

Lastly, for VE to be most successful for maintaining a building's sustainability, it is important VE be implemented at the very beginning and continues throughout the projects duration. VE can be mostly influenced during the conceptual planning, designing, and construction phases. It is important that the site, energy, materials, water, indoor environment quality, operation and maintenance, and even contracts are geared towards finding the best possible way to ensure a building's sustainability.

With the lessening of natural resources, the construction industry should really use value engineering to its fullest capability with helping buildings become more energy efficient and environmentally friendly.

STRUCTURAL BREADTH

Redesign of Foundation Wall

BACKGROUND

As stated earlier, the Health Care Center is going for LEED certification. This is not only a stepping stone for future buildings for the boarding school but for future medical facilities that lean towards better sustainability. The south addition has a six inch concrete foundation wall that extends in height from three feet below grade to the top of the first floor, a total of sixteen feet. A pitched roof rests on top of the first floor elevation. This design was chosen due to the good thermal insulation of concrete. The better the insulation the less amount of energy will be used which will result in cheaper energy bills. This is very important to medical facilities, like the Health Care Center, which consume an exuberant amount of energy on any given day.

PROBLEM

The foundation wall that extends a total height of 16 feet will be placed around the entire footprint of the lower half of the south addition (see Figure 8 below). An extensive amount of concrete will have to be poured to construct the foundation wall. This poses a great amount of problems in cost and in the schedule. Along with the cost of the concrete, costs for placing/pouring, forming and stripping the concrete are included. These factors mean more labor, which means a longer duration extending the overall length of the project.



Figure 8 - Cast-in-place concrete foundation wall location. Red indicates location of wall.

PROPOSAL

Through value engineering, an alternative solution of redesigning the concrete foundation wall out of unreinforced CMU (concrete masonry unit also known as concrete block) will be analyzed. The analysis will include a comparison of the original design and the new proposed design in the areas of construction costs and schedule reduction. A thermal comparison showing the difference in R-values between the two designs will also be included. This should show that the block wall design can still meet sustainability criteria by not being significantly lower than the concrete wall's R-value. R-values measure the resistance to heat flow, the higher the R-value, the less heat loss.

GOALS

The goal of the proposed analysis is to show that the new design of the CMU wall can save construction costs and even shorten the duration of the Health Care Center while maintaining its sustainable status. This should also show that by using value engineering, alternative solutions can be evaluated to determine if they can significantly impact the overall cost and schedule of a project without affecting a building's sustainable design and function.

ANALYSIS

Original Design

The original design of the concrete foundation wall is shown below (see Figure 9). The 1' x 2' footing rests three feet below the frost depth elevation. The six inch concrete wall that extends 16 feet up to the roof level is reinforced accordingly. Included with the concrete wall are two, two and a half inch rigid insulation boards, a two inch air gap, and four inch thick brick veneer.



Figure 9 - Drawing of original concrete design, not to scale.

CMU Design

When starting the design, the following assumptions were made.

Assumptions

- The brick veneer is non-loading bearing and will only have to support its self weight.
- The wall's self weight is 100 psf. The self weight x height of the wall = the total weight of the wall.

- Total weight of the wall = 100 psf x 16 ft = 1.6 kip
- Proper installation and function of a drainage system will prevent hydrostatic pressure and uplift forces.

The next thing determined was the total load acting on the wall. To find the load, a structural analysis of the pitched roof (Figure 10) was performed using STAAD Pro (a structural analysis computer program). The following are assumptions used for the roof analysis.





Assumptions

Roof Dead Loads					
Assupmtions	PSF				
Shingles	2				
Insulation	1				
Plywood	3				
Felt	2				
Total	8				

• The load will be acting directly in the center of the wall, preventing any moments cause by eccentricity.

- Arbitrary width, $A_t = 11.5$ ft
- Roof Dead Load = A_t x total psf = 11.5 ft x 8 psf = 92 plf (pounds per linear foot)
- Length of beam x roof dead load = 25 ft x 92 plf = 2300 lbs
- The C-channels that make up part of the roof structure were turned into point loads.
- Self weight of C-Channel = $11.5 \text{ plf x } A_t = 11.5 \text{ plf x } 15 \text{ ft} = 172.5 \text{ lbs}$
- The dead load was then turned into point loads along the length of the beam and placed on top of the points loads created by the C-channels. See Appendix B for all calculations.
- Through the structural analysis, the load acting on the foundation wall was found to be 1.5 kips.

The empirical design of concrete masonry walls, which is a conservative method to design a masonry wall, was used to find what the CMU size needed to be to support the roof load of 3.1 kips (self weight of wall + roof load). By using empirical design, vertical and lateral load resistance is governed by prescriptive criteria which include wall height to thickness ratios, shear wall length and spacing, minimum wall thickness, maximum building height, and other criteria, which has been proven effective through years of experience.

Empirical Design of Concrete Masonry Walls

- Height / thickness = $18 \Rightarrow 16$ ft (12inches) / t = 18, solve fort, t = 10.667.
- A 10 inch CMU block would be too small, so a 12 inch block will be used.
- Tables from R.S. Means were used to double check (Figure 11).

		Earthquak	ce Zones 0 & 1 Only	Allowable Vertical Wall Loads					Allowable Wall Moments (Without Vertical Wall Loads)			
Thk. T	Length Or Height			Eccentric Loads		Without Wind or	With Wind		Not Wind or Earthquake		Wind or Earthquake	
(Nom.) (in)	h′ (Ft.)	h′/t (in/in)	Type of Wall	7.0 (K/Ft.)	3.5 (K/Ft.)	Eccentric Loads (K/Ft.)	15 psf (K/Ft.)	30 psf (K/Ft.)	Inspe No (in-K/Ft.)	ction Yes (in-K/Ft.)	Inspe No (in-K/Ft.)	ection Yes (in-K/Ft.)
12"	8′	8	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	12.30 18.50 7.85 5.50	14.10 20.30 9.10 7.80	15.90 22.10 10.40 10.05	15.90 22.10 10.40 10.05	15.90 22.10 10.40 10.05	2.70 1.60 1.10 1.35	5.40 3.20 2.25 2.70	3.60 2.15 1.50 1.80	7.20 4.30 3.00 3.60
	12′	12	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	12.05 13.45 7.65 5.40	13.80 14.75 8.90 7.65	15.55 16.05 10.15 9.85	15.55 16.05 10.15 9.85	15.55 16.05 10.15 9.05	2.70 1.60 1.10 1.35	5.40 3.20 2.25 2.70	3.60 2.15 1.50 1.80	7.20 4.30 3.00 3.60
	16′	16	Solid Brick Solid CM Units Hollow CM Units	11.55 17.35 7.35	13.20 19.05 8.55	14.90 20.70 9.75	14.90 20.70 9.75	14.35 20.70 9.05	2.70 1.60 1.10	5.40 3.20 2.25	3.60 2.15 1.50	7.20 4.30 3.00
			Brick & Hollow CMU	5.20	7.30	9.75	9.75	9.05	1.10	2.25	1.5	30

Table B2010-116 Unreinforced Masonry Wall Capacities Per L.F. (Kips & In-Kips)

Figure 11 – R.S. Means load tables for masonry walls.

With 30 psf wind, a hollow twelve inch CMU block will be sufficient for the total load of 3 kips. The figure below shows the new wall design.



Figure 12 – Drawing of CMU foundation wall, not to scale.

Retention Wall

As seen in the last figure, part of the foundation wall will be acting as a retention wall. The wall sits down three feet below the frost line on the exterior of the wall. The interior wall extends down seven feet four inches into the soil. To make sure the twelve inch CMU wall is suitable, the moment acting on the wall due to the soil must be less then what the wall can handle. The following are steps used to find the moment.

Given

- Internal angle of friction, ϕ , = 28°
- Unit weight of soil, γ , = 130 pcf
- At Rest $K_0 = 1 \sin \phi = 0.53$
- $V = P => V = (K_o \gamma H^2)/2 = (0.53x130x7.25^2)/2 = 1810.8 \text{ ft-lb/ft}$
- Moment = (1810.8)(7.25/3) = 4376/1000 = 4.376 ft-K/ft = 0.364 in-K/ft

Table B2010-116 Unreinforced Masonry Wall Capacities Per L.F. (Kips & In-Kips)

	Earthquake Zones 0 & 1 Only				Allowabl	e Vertical Wa	all Loads	Allowable Wall Moments (Without Vertical Wall Loads)				
Thk. T	Length Or Height			Eccentric Loads		Without Wind or	With Wind		Not Wind or Earthquake		Wind or Earthquake	
(Nom.) (in)	h′ (Ft.)	h′/t (in/in)	Type of Wall	7.0 (K/Ft.)	3.5 (K/Ft.)	Eccentric Loads (K/Ft.)	15 psf (K/Ft.)	30 psf (K/Ft.)	Inspe No (in-K/Ft.)	ction Yes (in-K/Ft.)	Inspe No (in-K/Ft.)	ection Yes (in-K/Ft.)
12"	8'	8	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	12.30 18.50 7.85 5.50	14.10 20.30 9.10 7.80	15.90 22.10 10.40 10.05	15.90 22.10 10.40 10.05	15.90 22.10 10.40 10.05	2.70 1.60 1.10 1.35	5.40 3.20 2.25 2.70	3.60 2.15 1.50 1.80	7.20 4.30 3.00 3.60
	12′	12	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	12.05 13.45 7.65 5.40	13.80 14.75 8.90 7.65	15.55 16.05 10.15 9.85	15.55 16.05 10.15 9.85	15.55 16.05 10.15 9.05	2.70 1.60 1.10 1.35	5.40 3.20 2.25 2.70	3.60 2.15 1.50 1.80	7.20 4.30 3.00 3.60
	16′	16	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	11.55 17.35 7.35 5.20	13.20 19.05 8.55 7.30	14.90 20.70 9.75 9.45	14.90 20.70 9.75 9.10	14.35 20.70 9.05 —	2.70 1.60 1.10 1.35	5.40 3.20 2.25 2.70	3.60 2.15 1.50 1.80	7.20 4.30 3.00 3.60

Figure 13 – R.S. Means load tables for masonry walls.

Looking at the R.S. Means load tables, the maximum allowable wall moment for twelve inch CMU wall is 3 in-K/ft. This proves that the walls design is acceptable.

Thermal Comparison

When analyzing the two walls between their thermal insulation properties, they were actually close in value. As shown in the figure below, the original concrete foundation

wall design is comprised of two, two and a half inch rigid insulation boards, a two inch air gap, and four inch thick brick veneer. Their respective thermal resistance R-values is as follows.

Concrete Design						
Material	R value					
Outside Air Film	0.17					
4" Brick Veneer	0.8					
2" Air Gap	1					
2" Rigid Insulation Board	16					
6" Concrete Pour	0.48					
2" Rigid Insulation Board	16					
5/8" Gypsum Board	0.56					
Inside Air Film	0.68					
Total Thermal Resistance	35.69					

Figure 14 – Thermal properties of the concrete wall.

Similarly to the original design, the CMU foundation wall design has similar components. The only difference being that the six inch thick concrete is replaced by twelve inch CMU hollow block. The respective thermal resistance R-values is as follows for the new design.

CMU Design	
Material	R value
Outside Air Film	0.17
4" Brick Veneer	0.8
2" Air Gap	1
2" Rigid Insulation Board	16
8" CMU with Grout	1.81
2, 2" Rigid Insulation Board	16
5/8" Gypsum Board	0.56
Inside Air Film	0.68
Total Thermal Resistance	37.02

Figure 15 – Thermal properties of the CMU wall.

After comparing the two systems, the block wall has a higher R-value than the concrete wall. This proves that by using the CMU foundation wall design, no more heat loss will be lost than the original design. In fact, the CMU wall shows that less heat will be lost through heat transfer. Another factor deciding in if this alternative solution will be sustainable.

Cost Analysis

When comparing the cost between the two designs it's simple to see that the original design will cost more to construct than the CMU design. The main factor for this is the cost for more materials in the concrete design, and labor. A total of \$64,718 will be saved by switching to the CMU foundation wall design.

Concrete Design										
Concrete	Notes	Quantity	Unit	Material	Labor	Equipment	Total			
4000 psi		233	CY	84	0	0	19572			
Placing										
Pumped	Includes vibrating	233	CY	0	12.5	5	4077.5			
Forms										
Exterior walls 8'-16' 4 uses	Includes erecting, bracing, stripping & cleaning	23937	SFCA	0.7	4.05	0	113700.8			
Reinforcement										
Walls, #3 to #7		14.5	TON	760	405		16892.5			
Total Cost							154242.8			
CMU Design										
CMU Block	Notes	Quantity	Unit	Material	Labor	Equipment	Total			
12' hollow block		11968.5	SF	2.51	4.97		89524.38			
Total Cost							89524.38			

Figure 16 – Cost comparison between the two designs.

Also, the block wall design will take less labor and fewer crews to construct. The new design eliminates the need for a three crew process including a rebar crew for setting the reinforcement, a carpenter crew for the formwork, and the concrete crew for placing and vibrating the concrete. Only one group of masons needs to erect the CMU wall. By having one crew performing all the work, there will be no need for coordination between different crews and confusion due to the lack of coordination.

Schedule Analysis

As seen in Figure 18 on the next page, there will be a few days shed off of the schedule by using the CMU foundation wall design. The south addition was split into three sections, A, B and C (see Figure 17). There is more labor involved when constructing a concrete wall including, the formwork, rebar placement, and concrete placement. That is why there are a few days saved from the schedule. It seems nothing significant right now, but those few days will be used to start the steel erection earlier and can affect the overall duration of the project. Full scale schedule can be found in Appendix B.



Figure 17 - Foundation wall split in section A, B & C.



Figure 18 - Schedule comparison between cast-in-place concrete and CMU.
CONCLUSION

Through the value engineering analysis, the alternative solution to use twelve inch CMU block, replacing the cast-in-place concrete foundation wall seems very feasible. Through the design and engineering analysis, the un-reinforced CMU foundation wall will be structurally sound. The CMU will also act as better insulation, proving to have a higher R-value than the concrete wall. This higher R-value should have a good impact on the mechanical system in the building. It can be concluded that the sustainability of the Health Care Center has been maintained. When comparing costs, it's shown that a total of \$64,718 can be shed off of the project. Also, when comparing the durations between the two designs, the CMU foundation wall will be finished a few days earlier. This time can become beneficial in unforeseen delays that can occur later in the construction process. Through the analysis, the construction of a twelve inch un-reinforced CMU foundation wall is feasible and will maintain its sustainable value for the Health Care Center.

MECHANICAL BREADTH

Replacement of Domestic Water Supply Copper Piping with PEX Tubing **BACKGROUND**

Like most typical plumbing systems found in buildings, the Health Care Center relies extensively on copper piping for its domestic water supply. The domestic water supply enters the building from the basement level and splits into two directions. The one half starts to circulate through the basement level then up to the other levels continuing with the rest of the building. The other half enters the mechanical room where the water is either heated by one of the four water heaters or sent to another part of the building. The domestic water supply will then circulate throughout the building with the hot water supply re-circulating back to the hot water heaters and back again throughout the building.

PROBLEM

The price of copper in today's market is exceedingly high, and according to market trends (shown in the figures to the right) the price will not be decreasing any time soon. The price per pound has gone up over the past five years and has been increasing within the past couple months (to see the full scale of these charts please refer to Appendix C). In almost all of construction, commercial or residential, copper piping is used for plumbing. With the economic growth in Asia, China is buying up all the copper. This leads to plumbing systems



used in buildings to be more expensive. Another issue with using copper piping is the labor. The labor can become very extensive, thus time consuming, when it comes to running pipe around an angle or obstacle. It needs to be cut and a 90 degree elbow needs to be added. The Health Care Center is facing this issue right now with copper tubing.

As mentioned earlier, the building's domestic water supply is constructed out of copper piping. As a result the Health Care Center is not benefiting from the cost and duration of installing copper piping. The cost for copper piping and labor, not including all of the fittings and elbows used, is close to \$100,000.

PROPOSAL

The idea is to use value engineering to find a sustainable alternative to the problem identified in the previous paragraph so the Health Care Center can still maintain its LEED certification. The alternative chosen to replace the copper tubing is cross-linked

polyethylene, better know as PEX tubing. PEX will be replacing the copper pipes used for the domestic water supply in the building. A remote manifold system, which uses PEX tubing, will be used through out the building. Manifolds will be placed in locations around the building where groups of fixtures are located distributing the domestic water.



Figure 19 – Picture of PEX tubing.

GOALS

The goal of the proposed alternative design is to reduce material costs, labor costs, and energy costs for the Health Care Center by replacing the existing copper piping for domestic water with PEX tubing. This should also show that by using value engineering, sustainability can be maintained and in this case gained.

ANALYSIS

PEX piping has been successfully used in Europe for years before its use came over to America. It was originally used in residential and commercial construction for radiant floor heating and not until recently has PEX been used for plumbing systems. The following will include the advantages of using PEX tubing over copper and other rigid metals, the remote manifold system design, and a cost analysis for the domestic water supply in the Health Care Center.

<u>Advantages</u>

Ease of Installation

- PEX is manufactured in long coils which eliminate the need for coupling joints.
- The natural flexibility allows the piping to bend gently around obstructions minimizing the need for fittings.
- The pipe is lightweight making it easy to transport.

Durability

- PEX is not affected by reduced interior dimension, corrosion, filming, mineral buildup, and water velocity wear.
- It will expand when frozen then reach its original size when water thaws.

Cost Effective

- Lower installation time and labor time is greatly reduced.
- The use of water and energy is reduced by delivering the water to the fixtures faster and by reducing losses in the piping.

Energy Efficient

- PEX offers reduced heat loss and improved thermal characteristics.
- Less energy is used by the water heater because there is a shorter delivery time to the fixtures.

Noise Reduction

• Reduces occurrences of water hammer due to the flexibility and ability to absorb pressure surges.

Remote Manifold Design

There are a few systems that could have been chosen for the Health Care Center. There is an extensive amount of piping that needs to be installed from the basement, where the water heater and cold water supply line is located, to the entire building. For this reason the remote manifold system was chosen. The remote manifold system combines your typical branch plumbing system and the home-run system.

The Health Care Center will be split into four sections, a water heater for each section. These four sections include the first floor split into three sub-sections and the second

floor. Hot and cold water will be sent from the mechanical room, located in the basement, to their particular manifold (Figure 20 shown on the right) located around the building. From there the hot and cold water pipes will be split and sent off to individual fixtures. A couple of advantages to this design are that it will allow for a quicker hot water delivery during sequential flows, reduce the amount of fittings needed to be installed, and individual shut-off values located at the remote manifolds.



Figure 20 – PEX tubing and remote manifold.

The following AutoCAD drawings show the original plumbing design and the new PEX remote manifold design. In the drawings one can see exactly how the remote manifold system works. The four circles in the basement level represent the water heaters and the green box, \Box , signifies the manifolds. The red and blue lines that branch out of the manifold represent the PEX supply water traveling to fixtures. The red and blue lines that are extending out of the hot water tanks are still copper piping. All figures drawn are not to scale. In the First Floor Section B drawing, there was not enough space to show how the piping will be will be split from the remote manifold, so it is just assumed.

Original Design



PEX Design – Basement Level











PEX Design – Second Floor



PEX tubing is only manufactured in sizes shown in the table below. Due to the fact that PEX only comes in sizes two inches and smaller, the new design had to incorporate the smaller tubing. This was not a significant factor since the copper piping runs from the mechanical room to the manifolds, and most fixtures only need a 3/8 inch or 1/2 inch fitting. Copper tubing will still be used from the water heaters to the remote manifolds. PEX tubing will be used for the tubing from the manifold to the fixtures.

Nominal	OD	Wall	ID	Weight
Diameter	inches	inches ²	inches	lb/ft
3/8''	0.500	0.075	0.350	0.05
I/2"	0.625	0.075	0.475	0.06
3/4"	0.875	0.102	0.671	0.10
- I"	1.125	0.130	0.865	0.16
1 1/4"	1.375	0.160	1.055	0.25
1 1/2"	1.625	0.190	1.245	0.35
2"	2.125	0.248	1.629	0.60

Figure 21 – PEX Pipe Dimensions

The remote manifold design will have savings on energy and water consumption. The new design provides direct lines from the manifold to the fixtures, reducing the amount of water that goes through the pipes allowing less time for hot water to reach the fixture. In the design the direct lines were sized to the fixture requirements, further reducing the amount of time to wait for hot water. Faster hot water delivery reduces water waste and the amount of times the water heater must cycle to supply hot water. Another way the remote manifold system reduces water is by having fewer fittings. Fittings are only required at the fixtures and the manifold. This reduces the possibility of leaks, which wastes water and increases utility costs. The smoothness of the plastic tube also increases the flow of water, again making it quicker to reach the fixtures (see Appendix C for charts).

Cost Analysis

	Original Plumbing Design													
Copper Pipe	Quantity	Unit	Mat.	Mat. Total	MH	Tot. Hours	Total Cost							
Pipe, 1/2"	2366	LNFT	1.75	4140.5	0.06	142	12573.89							
Pipe, 3/4"	2251	LNFT	2.7	6077.7	0.06	135.1	14303.93							
Pipe, 1"	875	LNFT	3.84	3360	0.08	70	7653.32							
Pipe, 1-1/4"	1214	LNFT	5.4	6555.6	0.08	97.1	12692.18							
Pipe, 1-1/2"	722	LNFT	6.96	5025.12	0.08	57.8	8788.44							
Pipe, 2"	879	LNFT	10.96	9633.84	0.09	79.1	15066.97							
Pipe, 2-1/2"	681	LNFT	16.59	11297.79	0.12	81.7	17044.69							
Pipe, 3"	172	LNFT	22.26	3828.72	0.14	24.1	5571.98							
Pipe, 4"	80	LNFT	37.18	2974.4	0.18	14.4	4084.64							
Copper Fittings														
90 ELL, 1/2"	644	EACH	0.39	251.16	0.33	211.2	12205.63							
90 ELL, 3/4"	120	EACH	0.88	105.6	0.43	51.8	3043.27							
90 ELL, 1"	186	EACH	2.16	401.76	0.48	89.3	5484.1							
90 ELL, 1-1/4"	61	EACH	3.26	198.86	0.57	34.6	2175.49							
90 ELL, 1-1/2"	37	EACH	5.1	188.7	0.59	21.9	1444.33							
90 ELL, 2"	37	EACH	9.27	342.99	0.69	25.5	1814.79							
90 ELL, 2-1/2"	20	EACH	19.57	391.4	1.1	21.9	1668.26							
90 ELL, 3"	7	EACH	26.14	182.98	1.31	9.2	719.93							
90 ELL, 4"	4	EACH	66.92	267.68	1.75	7	690.21							
Total							127026.05							

Figure 22 – Material and labor costs for original design.

		Alternat	ive Plumbi	ng Design			
Copper Pipe	Quantity	Unit	Mat.	Mat. Total	MH	Tot. Hours	Total Cost
PEX Pipe, 1/2"	2	1000ft/COIL	364	728	0.06	138	9008
PEX Pipe, 1/2"	1	300ft/COIL	109	109			
PEX Pipe, 3/4"	4	500ft/COIL	299.95	1199.8	0.06	131	9059.8
PEX Pipe, 3/4"	1	300ft/COIL	178.5	178.5			
PEX Pipe, 1"	9	100ft/COIL	104.95	944.55	0.08	68	6384.55
PEX Pipe, 1-1/4"	4	300ft/COIL	749.95	2999.8	0.08	94	10519.8
PEX Pipe, 1-1/4"	1	100ft/COIL	279.95	279.95			
PEX Pipe, 1-1/2"	3	300ft/COIL	864.95	2594.85	0.08	56	7074.85
PEX Pipe, 1-1/2"	1	100ft/COIL	294.95	294.95			
Copper Pipe, 2"	879	LNFT	10.96	9633.84	0.09	79.1	15066.97
Copper Pipe, 2-1/2"	681	LNFT	16.59	11297.79	0.12	81.7	17044.69
Copper Pipe, 3"	172	LNFT	22.26	3828.72	0.14	24.1	5571.98
Copper Pipe, 4"	80	LNFT	37.18	2974.4	0.18	14.4	4084.64
Copper Fittings							
90 ELL, 2"	37	EACH	9.27	342.99	0.69	25.5	1814.79
90 ELL, 2-1/2"	20	EACH	19.57	391.4	1.1	21.9	1668.26
90 ELL, 3"	7	EACH	26.14	182.98	1.31	9.2	719.93
90 ELL, 4"	4	EACH	66.92	267.68	1.75	7	690.21
Total							88708.47

Figure 23 – Material and labor costs for new design.

When looking at the cost comparison between the two designs, the remote manifold design including PEX tubing will save \$38,317.58. This is a significant amount of

money that can be used in other areas of the project. Since PEX tubing is flexible, it can easily be bent around corners and obstructions eliminating the need for ninety degree elbow fittings. The elbow fittings alone will save \$29,246. That is a reason alone to switch to the new plumbing design. When consulting with a plumber, he stated that a factor of 0.0286 can be deducted for the labor on PEX tubing. With that information a total of 353.9 man hours will be saved. That will shorten the overall duration of the project.

CONCLUSION

Through value engineering, an alternative solution to the plumbing system in the Health Care Center was analyzed. The use of the remote manifold system using PEX piping was the intended solution. Through the evaluation, the new plumbing design will be successful. An overall cost of \$38,317.58 can be saved from the project cost and an approximate total of 354 man hours can be saved from the schedule. Most importantly, the Health Care Center will not loose any LEED points. Along with PEX's ability to reduce less energy used by the water heater, PEX tubing is also less toxic than the manufacturing of copper piping.

RECOMMENDATIONS

The following recommendations are from the interpretations and analyses from the two breadth topics covering the redesign of the foundation wall and the remote manifold plumbing system for the Health Care Center.

Both the structural and mechanical breadths were analyzed using value engineering. The purpose was to follow the considerations mentioned in the research topic to ensure that the Health Care Center would still maintain its LEED accreditation. The information in the research topic should be used for all buildings that are trying to strive for a sustainable status and going through the value engineering process.

Through the analysis and evaluation of the foundation wall, an un-reinforced twelve inch CMU foundation wall will be sufficient. To make certain that the wall will be structurally sound; the empirical design of concrete masonry walls was used. The wall was also checked for the moments acting on it due to pressure from the soil. This area was checked because approximately seven feet of the wall acts as a retention wall. After assuring the CMU wall would hold due to all of the forces acting on it, an analysis between the cost and duration of the wall was comprised. It has been found that the CMU wall costs approximately \$64,718 less and will take less time to construct. Lastly, keeping in mind that the buildings energy conservation should not be affected, a comparison between heat transfers was examined. The CMU wall has a higher R-value than the six inch concrete wall. With the new design having a higher R-value, energy will be saved from the mechanical system not having to compensate for the heat loss.

Through the analysis and evaluation of the plumbing system, the remote manifold system using PEX tubing is an appropriate solution. The remote manifold system including PEX tubing has proven many advantages over the typical branch system with copper tubing. The remote manifold system has the advantage of reducing heat loss due to the faster water flow from the water heater to the fixtures, easy shut off valves for individual fixtures without shutting the rest of the water off, and less water loss due to fewer fittings installed in the system. PEX tubing has shown its advantages of costing less than copper tubing, being able to bend around obstructions due to its flexibility, quicker water velocity due to the smoothness of the plastic, and creates fewer toxins than the manufacturing of copper. All of these reasons proving the remote manifold system, with the use of PEX piping, being energy and environmentally friendly. It is shown that the replacing of the plumbing system will save approximately \$38,317.58.

The final recommendation for the Health Care Center would be to implement the two proposed solutions. With both the CMU foundation wall and remote manifold plumbing system installed with PEX tubing maintaining the Health Care Center's LEED status, the value engineering performed was successful. The project will save over \$100,000 by switching to both of the alternative solutions and even shorten the total duration of the project.

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APPENDIX A

Project Overview-Research Topic



	QUESTIONNAIRE
1	How would you define value engineering (VE)?
2	Have you ever performed VE on a specific job?
	If so what type of project (ie. health care, office building, airport, education, etc)?
4	Is there a difference in VE and cutting costs?
5	Who should be involved in the VE process (ie. owner, architect, CM)?
6	When should VE occur?
	Should this change, if the building was going for LEED or some sustainability status?
7	How would VE for a sustainable building differ from a regular building?
8	What are the steps or logistical thinking process you take during VE?
	Can this be applied to sustainable buildings also? If not, what should be different?
10	What is first looked at when doing VE for a building?
11	How do you get the best results out of VE or evalutate the best alternatives?
12	How do you communicate these VE ideas?
13	How would you integrate VE and sustainability?
14	What is more important first cost or life cycle cost? Why?

15	How do you manage quality during VE?
16	Should there be any future follow up or implementation?
	If so how and what should be done?
18	How do you educate or get the information out about VE and sustainability?

APPENDIX B

Structural Breadth

PAGE NO.

1

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                       STAAD.Pro
            *
                       Version 2006
                                       Bld 1002.US
                       Proprietary Program of
                       Research Engineers, Intl.
                                APR 6, 2007
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                       Time=
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    3. ENGINEER DATE 31-MAR-07
    4. END JOB INFORMATION
    5. INPUT WIDTH 79
    6. UNIT FEET POUND
    7. JOINT COORDINATES
    8. 1 0 0 0; 2 38 0 0; 3 2 1.579 0; 4 36 1.579 0; 5 19 15 0; 6 12.5 1.579 0
    9. 7 25.5 1.579 0; 8 12.5 8.5 0; 9 25.5 8.5 0; 10 10.767 8.5 0; 11 27.233 8.5 0
   10. 12 5.102 4.028 0; 13 32.898 4.028 0; 14 10.008 7.901 0; 15 27.992 7.901 0
   11. 16 14.914 11.774 0; 17 23.086 11.774 0
   12. MEMBER INCIDENCES
   13. 3 3 4; 4 8 6; 5 10 11; 6 9 7; 7 11 7; 8 10 6; 9 1 3; 10 3 12; 11 12 14
   14. 12 14 10; 13 10 16; 14 16 5; 15 2 4; 16 4 13; 17 13 15; 18 15 11; 19 11 17
   15. 20 17 5
   16. DEFINE MATERIAL START
   17. ISOTROPIC STEEL
   18. E 4.176E+009
   19. POISSON 0.3
   20. DENSITY 489.024
   21. ALPHA 6.5E-006
   22. DAMP 0.03
   23. END DEFINE MATERIAL
   24. MEMBER PROPERTY AMERICAN
   25. 5 9 TO 20 TABLE ST W8X24
   26. 4 6 TO 8 TABLE ST C8X11
   27. 3 TABLE ST MC8X22
   28. CONSTANTS
   29. MATERIAL STEEL ALL
   30. SUPPORTS
   31. 3 6 7 PINNED
   32. 4 FIXED BUT FX MZ
   33. LOAD 1 LOADTYPE NONE TITLE LOAD CASE 1
   34. JOINT LOAD
   35. 1 2 12 TO 17 FY -126.5
   36. 5 FY -165
   37. 1 2 FY -299
   38. 12 13 FY -586.5
   39. 14 15 FY -575
   40. 16 17 FY -563.5
```

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41. 5 FY -552
42. PERFORM ANALYSIS

PROBLEM STATISTICS

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS =17/18/4ORIGINAL/FINAL BAND-WIDTH=12/4/27 DOFTOTAL PRIMARY LOAD CASES =1, TOTAL DEGREES OF FREEDOM =89SIZE OF STIFFNESS MATRIX =3 DOUBLEKILO-WORDSREQRD/AVAIL. DISK SPACE =12.1/137514.5 MB

43. LOAD LIST ALL44. PRINT SUPPORT REACTION ALL

-- PAGE NO. 3

SUPP	ORT RE	ACTIONS -UN	NIT POUN FE	SET STRU	CTURE TYPE	= SPACE	
JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
3 6 7 4	1 1 1 1	4.40 -361.79 357.38 0.00	1458.95 1429.78 1429.04 1459.23	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00

*************** END OF LATEST ANALYSIS RESULT *****************

45. PRINT MAXFORCE ENVELOPE ALL

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MEMBER FORCE ENVELOPE

ALL UNITS ARE POUN FEET

MAX AND MIN FORCE VALUES AMONGST ALL SECTION LOCATIONS

MEMB		FY/	DIST	LD	MZ/	DIST	LD			
		FΖ	DIST	LD	MY	DIST	LD	FX	DIST	LD
з	мах	0.25	0.00	1	-22.54	0.00	1			
5	1 11 12 1	0.00	0 00	1	0 00	0 00	1	649 40 т	0 00	1
	MIN	0.00	34 00	1	-31 19	34 00	1	019.10 1	0.00	-
	MILIN	0.25	34.00	1	0 00	34.00	1	649 40 T	34 00	1
		0.00	51.00	-	0.00	51.00	1	019.10 1	51.00	-
4	MAX	0.00	0.00	1	0.00	0.00	1			
		0.00	0.00	1	0.00	0.00	1	0.00	0.00	1
	MIN	0.00	6.92	1	0.00	6.92	1			
		0.00	6.92	1	0.00	6.92	1	0.00	6.92	1
5	MAX	-0.01	0.00	1	22.96	16.47	1			
		0.00	0.00	1	0.00	0.00	1	560.66 T	0.00	1
	MIN	-0.01	16.47	1	22.72	0.00	1			
		0.00	16.47	1	0.00	16.47	1	560.66 T	16.47	1
б	MAX	0.00	0.00	1	0.00	6.34	1			
		0.00	0.00	1	0.00	0.00	1	0.00	0.00	1
	MIN	0.00	6.92	1	0.00	0.00	1			
		0.00	6.92	1	0.00	6.92	1	0.00	6.92	1
7	MAX	-0.43	0.00	1	0.00	7.13	1			
		0.00	0.00	1	0.00	0.00	1	1473.05 C	0.00	1
	MIN	-0.43	7.13	1	-3.06	0.00	1			
		0.00	7.13	1	0.00	7.13	1	1473.05 C	7.13	1
8	MAX	3.66	0.00	1	26.14	0.00	1			
		0.00	0.00	1	0.00	0.00	1	1474.84 C	0.00	1
	MIN	3.66	7.13	1	0.00	7.13	1			
		0.00	7.13	1	0.00	7.13	1	1474.84 C	7.13	1
9	МАХ	-333.96	0.00	1	851.00	2.55	1			
		0.00	0.00	1	0.00	0.00	1	263.66 T	0.00	1
	MIN	-333.96	2.55	1	0.00	0.00	1			
		0.00	2.55	1	0.00	2.55	1	263.66 Т	2.55	1
10	MAX	405.80	0.00	1	873.54	0.00	1			
		0.00	0.00	1	0.00	0.00	1	1153.38 C	0.00	1
	MIN	405.80	3.95	1	-730.27	3.95	1			
		0.00	3.95	1	0.00	3.95	1	1153.38 C	3.95	1
11	мах	-153.79	0.00	1	231.02	6.25	1			
		0.00	0.00	1	0.00	0.00	1	711.57 C	0.00	1

Friday,	April	06,	2007,	10:02	ΡM
,		/	,		

ST.	AAD SF	PACE						PAGE	NO.	5
	MIN	-153.79	6.25	1	-730.27	0.00	1			
		0.00	6.25	1	0.00	6.25	1	711.57 C	6.25	1
12	MAX	-704.36	0.00	1	912.05	0.97	1			
		0.00	0.00	1	0.00	0.00	1	277.01 C	0.00	1
	MIN	-704.36	0.97	1	231.02	0.00	1			
		0.00	0.97	1	0.00	0.97	1	277.01 C	0.97	1
13	MAX	294.57	0.00	1	863.20	0.00	1			
		0.00	0.00	1	0.00	0.00	1	1318.94 C	0.00	1
	MIN	294.57	5.28	1	-693.22	5.28	1			
		0.00	5.28	1	0.00	5.28	1	1318.94 C	5.28	1
14	MAX	-247.01	0.00	1	592.73	5.21	1			
		0.00	0.00	1	0.00	0.00	1	891.38 C	0.00	1
	MIN	-247.01	5.21	1	-693.22	0.00	1			
		0.00	5.21	1	0.00	5.21	1	891.38 C	5.21	1
15	MAX	-333.96	0.00	1	851.00	2.55	1			
		0.00	0.00	1	0.00	0.00	1	263.66 T	0.00	1
	MIN	-333.96	2.55	1	0.00	0.00	1			
		0.00	2.55	1	0.00	2.55	1	263.66 T	2.55	1
16	MAX	409.15	0.00	1	882.19	0.00	1			
		0.00	0.00	1	0.00	0.00	1	1150.41 C	0.00	1
	MIN	409.15	3.95	1	-734.86	3.95	1			
		0.00	3.95	1	0.00	3.95	1	1150.41 C	3.95	1
17	MAX	-150.44	0.00	1	205.49	6.25	1			
		0.00	0.00	1	0.00	0.00	1	708.60 C	0.00	1
	MIN	-150.44	6.25	1	-734.86	0.00	1			
		0.00	6.25	1	0.00	6.25	1	708.60 C	6.25	1
18	MAX	-701.01	0.00	1	883.29	0.97	1			
		0.00	0.00	1	0.00	0.00	1	274.04 C	0.00	1
	MIN	-701.01	0.97	1	205.49	0.00	1			
		0.00	0.97	1	0.00	0.97	1	274.04 C	0.97	1
19	MAX	294.59	0.00	1	863.39	0.00	1			
		0.00	0.00	1	0.00	0.00	1	1318.96 C	0.00	1
	MIN	294.59	5.28	1	-693.12	5.28	1			
		0.00	5.28	1	0.00	5.28	1	1318.96 C	5.28	1
20	MAX	-246.99	0.00	1	592.73	5.21	1			
		0.00	0.00	1	0.00	0.00	1	891.39 C	0.00	1
	MIN	-246.99	5.21	1	-693.12	0.00	1			
		0.00	5.21	1	0.00	5.21	1	891.39 C	5.21	1

********* END OF FORCE ENVELOPE FROM INTERNAL STORAGE *********

46. FINISH

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********** END OF THE STAAD.Pro RUN ********** **** DATE= APR 6,2007 TIME= 22: 0:11 **** For questions on STAAD.Pro, please contact * * * Research Engineers Offices at the following locations Telephone Email support@reiusa.com * USA: +1 (714)974-2500 * CANADA +1 (905)632-4771 detech@odandetech.com * * CANADA +1 (604)629 6087 staad@dowco.com * +44(1454)207-000support@reel.co.uk UK * FRANCE +33(0)1 64551084 support@reel.co.uk +49/931/40468-71 * GERMANY info@reig.de * NORWAY +47 67 57 21 30 staad@edr.no * SINGAPORE +65 6225-6015/16 support@reiasia.net * * INDIA +91(033)2357-3575 support@calcutta.reiusa.com * * JAPAN +81(03)5952-6500 eng-eye@crc.co.jp * CHINA +86(411)363-1983 support@reiasia.net * THAILAND +66(0)2645-1018/19 support@thai.reiusa.com * * North America support@reiusa.com * Europe support@reel.co.uk * Asia support@reiasia.net ****

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Information about the key files in the current distribution

Modification	Date CRC	Size (Bytes)	File Name
07/18/2006	0x3881	13000704	SProStaad.exe
07/18/2006	0x100	05738496	SProStaadStl.exe
09/19/2003	0x2fc0	00081970	CMesh.dll
05/31/2006	0x3c0	02486272	dbSectionInterface.dll
01/24/2001	0x9b40	00073728	LoadGen.dll
09/25/2003	0x6340	00704512	MeshEngine.dll
09/22/2003	0xce00	00069632	QuadPlateEngine.dll
12/22/2005	0x4181	00094208	SurfMesh.dll
01/03/2006	0x81c1	00493568	aiscsections.mdb
06/13/2006	0xd4c1	01204224	AISCSectionsRCeco.mdb
01/05/2005	0x79c1	00319488	aiscsections_all_editions.mdb
01/05/2005	0x4b81	01810432	aiscsteeljoists.mdb
01/05/2005	0xcac1	03651584	aitctimbersections.mdb
01/27/2005	0xeb01	00552960	aluminumsections.mdb
01/05/2005	0xcd01	00163840	australiansections.mdb
01/05/2005	0x6a41	00229376	britishsections.mdb
07/08/2005	0x9d41	00434176	bscoldformedsections.mdb
06/28/2005	0x8201	00327680	butlercoldformedsections.mdb
01/05/2005	0xabc0	00262144	canadiansections.mdb
05/31/2005	0x9e81	00450560	canadiantimbersections.mdb
06/09/2006	0x1f81	00774144	ChineseSections.mdb
01/05/2005	0xd6c0	00600064	dutchsections.mdb
01/05/2005	0x1a00	00354304	europeansections.mdb
01/05/2005	0xd301	00202752	frenchsections.mdb
01/05/2005	0x11c1	00233472	germansections.mdb
01/05/2005	0x3c40	00264192	indiansections.mdb
01/05/2005	0xd540	00180224	iscoldformedsections.mdb
03/23/2006	0xa080	00200704	japanesesections.mdb
11/09/2005	0x9081	00376832	Kingspancoldformedsections.mdb
01/05/2005	0xb740	00174080	koreansections.mdb
02/03/2005	0xda00	00096256	lysaghtcoldformedsections.mdb
02/07/2005	0x9a00	00243712	mexicansteeltables.mdb
06/13/2006	0x3501	00421888	RCecoColdFormedSections.mdb
02/03/2005	0x9b40	00307200	russiansections.mdb
01/05/2005	0x9081	00206848	southafricansections.mdb
01/06/2005	0x9341	00194560	spanishsections.mdb
01/04/2006	0x8680	00223232	uscoldformedsections.mdb
01/05/2005	0xbac0	00149504	usersectionstemplate.mdb
01/20/2006	0x8e40	00159744	venezuelansections.mdb



Table B2010-112 Partially and Fully Grouted Reinforced Concrete Masonry Wall Capacities Per L.F. (Kips & In-Kips)

	Earthqu	ake Zones	1, 2 & 3					Allowable	e Vertical W	/all Loads		Allowable Wall Moments				
The	Lei (ngth Or	Groute	d Core		Eccentria Loodo			Withou	ıt Wind		With Wind		(without Wall L	oads)	•
тпк.	не		& K	ebar	7.0 in	Eccentr I-K/Ft.	3.5 in	I-K/Ft.	or Eccentric Loads Inspectio			Inspection	ection		/ind or quake	3
T (Nom.) (in)	h′ (Ft.)	h′/T (in/in)	(spac- ing) (in O.C.)	Rebar Size (@ dL)	Inspection No Yes (K/Ft.) (K/Ft.)		Inspe No (K/Ft.)	Inspection No Yes (K/Ft.) (K/Ft.)		ection Yes (K/Ft.)	N 15 psf (K/Ft.)	lo 30 psf (K/Ft.)	Yes 15 & 30 (K/Ft.)	Inspe No (inK/Ft.)	ection Yes (inK/Ft.)	SHE
8" Conc. Block	8′	12	48" 32" 16" 8"	#8 #5 ↓	5.10 5.45 6.50 10.10	12.55 13.35 15.80 23.40	6.25 6.65 7.90 11.70	13.70 14.60 17.15 25.00	7.75 7.90 9.25 13.30	14.90 15.80 18.50 26.55	7.45 7.90 9.25 13.30	7.45 7.90 9.25 13.30	14.90 15.80 18.50 26.55	7.55 6.45 7.95 10.20	12.20 9.60 12.85 17.15	
	12′	18	48" 32" 16" 8"	#8 #5 ↓	4.70 5.05 6.00 9.30	11.60 12.35 14.55 21.60	5.80 6.15 7.30 10.80	12.65 13.45 15.85 23.05	6.85 7.30 8.55 12.25	13.75 14.60 17.10 24.55	6.85 7.30 8.55 12.25	6.85 7.30 8.55 12.25	13.75 14.60 17.10 24.55	7.55 6.45 7.95 10.20	12.20 9.60 12.85 17.15	
	16′	24	48" 32" 16" 8"	#8 #5 ↓	3.95 4.20 5.05 7.80	9.70 12.25 12.20 18.10	4.85 5.15 6.10 9.05	10.60 11.30 13.30 19.35	5.75 6.10 7.15 10.30	11.55 12.25 14.35 20.60	5.75 6.10 7.15 10.30	— — — 9.65	11.55 12.25 14.35 20.60	7.55 6.45 7.95 10.20	12.20 9.60 12.85 17.15	
10" Conc. Block	8′	9.6	48" 32" 16" 8"	#8 ↓ #5 ↓	7.25 7.80 9.45 14.50	16.45 17.60 21.15 31.65	8.20 8.80 10.55 15.80	17.40 18.60 22.25 32.95	9.15 9.80 11.65 17.10		9.15 9.80 11.65 17.10	9.15 9.80 11.65 17.10	18.35 19.55 23.35 34.25	13.10 14.55 13.90 18.45	21.05 24.15 22.35 30.15	
	12	14.4	48" 32" 16" 8"	#8 ↓ #5 ↓	7.05 7.60 9.20 14.10	16.00 17.10 20.55 30.75	8.00 8.55 10.25 15.35	16.90 18.05 21.60 32.05	8.90 9.50 11.35 16.65	17.85 19.05 22.70 33.00	8.90 9.50 11.35 16.65	8.90 9.50 11.35 16.65	17.85 19.05 22.70 33.30	13.10 14.55 13.90 18.35	21.05 24.15 22.35 30.15	
	16′	19.2	48" 32" 16" 8"	#8 ↓ #5 ↓	6.70 7.15 8.70 13.35	15.10 16.15 19.40 29.05	7.55 8.05 9.70 14.50	16.00 17.05 20.40 30.25	8.40 9.00 10.70 15.70	16.85 17.95 21.45 31.45	8.40 9.00 10.70 15.70	8.40 9.00 10.70 15.70	16.85 17.95 21.45 31.45	13.10 14.55 13.90 18.35	21.05 24.15 22.35 30.15	
	20′	24	48" 32" 16" 8"	#8 ↓ #5 ↓	6.05 6.45 7.85 12.05	13.65 14.60 17.50 26.25	6.80 7.30 8.75 13.10	14.45 15.40 18.45 27.30	7.60 8.10 9.65 14.20	15.20 16.25 19.35 28.40	7.60 8.10 9.65 14.20	— 0.70 0.25 13.40	15.20 16.25 19.35 28.40	13.10 14.55 13.90 18.35	21.05 24.15 22.35 30.15	
12" Conc. Block	8′	8	48" 32" 16" 8"	#8 ↓ #5 ↓	9.20 9.90 12.10 18.60	20.00 21.50 26.05 39.35	10.00 10.75 13.00 19.65	20.75 22.30 26.95 40.40	10.75 11.55 13.90 20.75	21.55 23.15 27.85 41.50	10.75 11.55 13.90 20.75	10.75 11.55 13.90 20.75	21.55 23.15 27.85 41.50	15.30 17.10 16.20 21.45	24.40 28.10 25.90 35.10	S.
	12′	12	48" 32" 16" 8"	#8 ↓ #5 ↓	9.00 9.70 11.85 18.20	19.55 21.05 25.50 38.50	9.75 10.50 12.75 19.25	20.35 21.85 26.40 39.55	10.55 11.30 13.65 20.30	21.10 22.65 27.30 40.60	10.55 11.30 13.65 20.30	10.55 11.30 13.65 20.30	21.10 22.65 27.30 40.60	15.30 17.10 16.20 21.45	24.40 28.10 25.90 35.10	NCE NO
	16′	16	48" 32" 16" 8"	#8 ↓ #5 ↓	8.65 9.30 11.35 17.45	18.75 20.15 24.40 36.90	9.35 10.05 12.20 18.45	19.50 20.90 25.25 37.90	10.10 10.85 13.05 19.45	20.20 21.70 26.15 38.90	10.10 10.85 13.05 19.45	10.10 10.85 13.05 19.45	20.20 21.70 26.15 38.90	15.30 17.10 16.20 21.45	24.40 28.10 25.90 35.10	REFERE
	24′	24	48" 32" 16" 8"	#8 ↓ #5 ↓	7.05 7.60 9.30 14.30	15.35 16.55 20.00 30.25	7.65 8.25 10.00 15.10	15.95 17.15 20.70 31.10	8.30 8.90 10.70 15.95	16.55 17.80 21.45 31.90	8.30 8.90 10.40* 15.55*	— — — 15.15	16.55 17.80 21.45 31.90	15.30 17.10 16.20 21.45	24.40 28.10 25.90 35.10	

*Zone 3 only

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Table B2010-114 Fully Grouted Reinforced Masonry Wall Capacities Per L.F. (Kips & In-Kips)

	Earthqu	ake Zones	1, 2 & 3		Allowable Vertical Wall Loads									Allov Wall M	vable oments	
	Ler (ngth Dr	Туре						Withou	ıt Wind		With Wind		Without	Vertical Loads	
Thk.	He	ight	Wall	Rebar		Eccentri	ic Loads	14 /00-	or Eco	centric					Not Wind or	
					7.0 ir	i-K/Ft.	3.5 ir	i-K/Ft .	Loa	ads		Inspection		Earthquake		
			Brick	Size	Incod	oction	Inena	oction	Inche	oction		lo	Vac	Incne	action	
(Nom)	h′	h/Л	Grout	and	No	Yes	No	Yes	No	Yes	15 nsf	30 nsf	15 & 30	No	Yes	
(in)	(Ft.)	(in/in)	M.U.	(in. O.C.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(K/Ft.)	(inK/Ft.)	(inK/Ft.)	
8"			4"0"4"	#5@32	10 10	23 35	11 70	24 50	13 30	26 55	13 30	13 30	26 55	6.90	9.65	
Ŭ	8′	12	Solid CMU	INCOL	12.75	28.70	14.35	30.30	15.95	31.90	15.95	15.95	31.90	7.80	9.75	
	1.0.	10	4"0"4"		9.30	21.60	10.80	23.05	12.25	24.55	12.25	12.25	24.55	6.90	9.65	
	12'	18	Solid CMU		16.65	26.50	18.15	28.00	14.70	29.45	14.70	14.70	29.45	7.80	9.75	
	10	24	4"0"4"		7.80	18.10	9.05	19.35	10.30	20.60	10.30	9.65	20.60	6.90	9.65	
	10	24	Solid CMU	•	9.85	22.20	11.10	23.45	12.35	24.70	12.35	12.35	12.70	7.80	9.75	
10″			4″0″6″	#5@24	14.45	31.50	15.75	32.80	17.05	34.10	17.05	17.05	34.10	11.20	16.20	
	8′	9.6	Solid CMU		17.85	38.35	19.15	39.65	20.45	40.90	20.45	20.45	40.90	12.65	16.35	
			4"2"4"		14.45	31.50	15.75	32.80	17.05	34.10	17.05	17.05	34.10	11.20	16.20	
			4"0"6"		13.90	30.35	15.15	31.60	16.40	32.80	16.40	16.40	32.80	11.20	16.20	
	12′	14.4	Solid CMU		17.20	36.90	18.45	38.15	19.70	39.40	19.70	19.70	39.40	12.65	16.35	
			4"2"4"		13.90	30.35	15.15	31.60	16.40	32.80	16.40	16.40	32.80	11.20	16.20	
			4″0″6″		12.85	28.05	14.00	29.20	15.15	30.35	15.15	15.15	30.35	11.20	16.20	
	16′	19.2	Solid CMU		15.90	34.10	17.05	35.25	18.20	36.40	13.20	13.20	36.40	12.65	16.35	
			4"2"4"		12.85	23.05	14.00	29.20	15.15	30.35	15.15	15.15	30.35	11.20	16.20	
			4"0"6"		11.15	24.25	12.10	25.25	13.10	26.20	13.10	12.40	26.20	11.20	16.20	
	20'	24	Solid CMU		13.75	29.50	14./5	30.50	15./5	31.50	15./5	15./5	31.50	12.65	16.35	
1.0"			4"2"4"	♥	11.15	24.25	12.10	25.25	13.10	26.20	13.10	12.40	26.20	11.20	16.20	
12"	0/		4"0"8"	#8@48	18.60	39.35	19.65	40.40	20.75	41.50	20.75	20.75	41.50	10.05	24.90	
	8'	× ×		#5@00	22.75	47.65	23.80	48.70	24.90	49.80	24.90	24.90	49.80	18.80	25.10	
			4"2"0"	#9@20	10.00	39.30	19.00	40.40	20.75	41.50	20.75	20.75	41.50	11.90	18.75	
	1.07	10		#8@48	18.20	38.50	19.20	39.00	20.30	40.60	20.30	20.30	40.60		24.90	
	12	12		₩ 5@20	10.20	40.00	23.30	20.55	24.50	40.75	24.50	24.50	40.75	11.00	20.10	
			420	#3@20	17.45	36.00	19.25	39.00	19.50	38.00	19.50	10.50	38.00	16.65	2/ 00	
	16'	16	Solid CMU	#0@40 ⊥	21 30	1/1 70	22 35	15 70	22 25	16 70	23.45	22 25	16 70	18.80	24.50	
	10		4"2"6"	#5@20	17.45	36.90	18.45	37.90	19.45	38.90	19.45	19.45	38.90	11 90	18 75	
			4"0"8"	#8@48	14 30	30.25	15.10	31 10	15.45	31.90	15.45	15.45	31.90	16.65	24.90	
	24'	24	Solid CMU	↓ ↓	17.15	36.65	18.30	37.45	19.15	38.30	19.15	19.15	38.30	18.80	25.10	
			4"2"6"	#5@20	14.30	30.25	15.10	31.10	15.95	31.90	15.95	15.15	31.90	11.90	18.75	
16″			4"0"12"	#8@32	26.40	54.40	27.20	55.20	28.00	56.05	28.00	28.00	56.05	31.20	49.10	
	8′	6	Solid CMU	↓	32.00	65.65	32.80	66.45	33.60	67.25	33.60	33.60	67.25	35.25	50.40	
			4"2"10"	#5@15	26.40	54.40	27.20	55.20	28.00	56.05	28.00	28.00	56.05	14.75	24.10	
			4"0"12"	#8@32	26.15	53.95	26.95	54.75	27.75	55.55	27.75	27.75	55.55	31.20	49.10	
	12′	9	Solid CMU	₩	31.70	66.05	32.50	65.85	33.30	66.65	33.00	33.30	66.65	35.25	50.40	
			4"2"10"	#5@15	26.15	53.95	26.95	54.75	27.75	55.55	27.75	27.75	55.55	14.75	24.10	
			4″0″12″	#8@32	25.70	53.05	26.50	53.80	28.30	54.60	27.30	27.30	54.60	31.20	49.10	
	16′	12	Solid CMU		31.20	63.95	31.95	64.75	32.75	65.50	32.75	32.75	65.50	35.25	50.40	
			4"2"10"	+	25.70	53.05	26.50	53.80	27.30	54.60	27.30	27.30	59.60	14.75	24.10	
			4"0"12"	#8@32	20.35	41.95	20.95	42.55	21.60	43.20	18.75*	18.75*	43.20	31.20	49.10	
	32′	24	Solid CMU	. ↓	24.65	50.60	25.30	51.20	25.90	51.85	24.55*	24.55*	51.85	35.25	50.40	
			4″2″10″	#5@15	20.35	41.95	20.95	42.55	21.60	43.20	18.75*	18.75*	43.20	14.75	24.10	
*7 20	. 1	•	•											:		

*Zone 3 Only

Table B2010-116 Unreinforced Masonry Wall Capacities Per L.F. (Kips & In-Kips)

		Earthquak	e Zones 0 & 1 Only		Allowabl	e Vertical W	all Loads	Allowable Wall Moments (Without Vertical Wall Loads)				
Thk. T	Length Or Height			Eccentric Loads		Without Wind or	With Wind		Not Wind or Earthquake		Wind or Earthquake	
(INOM.)	h /	h//h	Time of	70	25	Eccentric	1E nof	20 maf	Inspe	ection	Inspe	ction
(111)	(Ft.)	(in/in)	Wall	/.0 (K/Ft.)	3.5 (K/Ft.)	(K/Ft.)	15 psr (K/Ft.)	30 psr (K/Ft.)	(in-K/Ft.)	in-K/Ft.)	(in-K/Ft.)	in-K/Ft.)
8″	8′	12	Solid Brick Solid CM Units	4.85 8.85 7.05	7.50 11.50	10.15 14.15	10.15 14.15	10.15 14.15	1.15 .70	2.30 1.40	1.55 .95	3.10 1.85
	10′	15	Solid Brick Solid CM Units Hollow CM Units	4.70 8.55	7.30	9.85 13.75 6 30	9.85 13.75 6 30	9.85 13.75 6.05	1.15 .70 .45	2.30 1.40	1.55 .90	3.10 1.85 1.25
	12′	18	Solid Brick Solid CM Units	8.15	6.95 10.60	9.40 13.10	9.40 13.10	7.95 12.90	1.15 .70	2.30 1.40	1.55 .90	3.10 1.85 1.25
12"	8′	8	Solid Brick Solid CM Units Hollow CM Units	12.30 18.50 7.85	4.25 14.10 20.30 9.10	15.90 22.10 10.40	15.90 22.10 10.40	4.75 15.90 22.10 10.40	2.70 1.60 1.10	5.40 3.20 2.25	3.60 2.15 1.50	7.20 4.30 3.00
	12'	12	Solid Brick Solid CM Units Hollow CM Units	5.50 12.05 13.45 7.65	7.80 13.80 14.75 8.90	15.55 16.05 10.15	15.55 16.05 10.15	15.55 16.05 10.15	2.70 1.60 1.10	5.40 3.20 2.25	3.60 2.15 1.50	7.20 4.30 3.00
	16′	16	Solid Brick Solid CM Units Hollow CM Units Prick & Hollow CMU	5.40 11.55 17.35 7.35 5.20	7.65 13.20 19.05 8.55 7.20	9.85 14.90 20.70 9.75 0.45	9.85 14.90 20.70 9.75 0.10	9.05 14.35 20.70 9.05	2.70 1.60 1.10 1.25	5.40 3.20 2.25 2.70	3.60 2.15 1.50	3.60 7.20 4.30 3.00 2.60
16″	12′	9	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	18.60 26.95 10.85 9.30	19.95 28.30 12.10	21.30 29.60 13.30 12.85	21.30 29.60 13.30 12.85	21.30 29.60 13.30 12.85	4.85 2.90 1.50 2.20	9.75 5.85 3.05	6.50 3.90 2.00	13.00 7.80 4.05 5.85
	16′	12	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	18.30 26.50 10.70 9.15	19.60 27.80 11.90 10.90	20.90 29.10 13.10 12.65	20.90 29.10 13.10 12.65	20.90 29.10 13.10 11.10	4.85 2.90 1.50 2.20	9.75 5.85 3.05	6.50 3.90 2.00 2.90	13.00 7.80 4.05 5.85
	20′	15	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	17.80 25.75 10.40 8.90	19.05 27.00 11.55 10.60	20.30 28.25 12.70 12.30	20.30 28.25 12.70 12.00	20.30 28.25 10.95	4.85 2.90 1.50 2.20	9.75 5.85 3.05 4.40	6.50 3.90 2.00 2.90	13.00 7.80 4.05 5.85
20″	12′	7.2	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	24.80 35.30 16.15 16.10	25.85 36.40 17.15 17.25	26.90 37.45 18.15 18.45	26.90 37.45 18.15 18.45	26.90 37.45 18.15 18.45	7.70 4.60 2.50 4.05	15.40 9.20 5.05 8.10	10.25 6.15 3.35 5.40	20.50 12.30 6.75 10.80
	16′	9.6	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	24.55 35.00 16.00 15.95	25.60 36.10 17.00 17.10	26.70 37.15 18.00 18.30	26.70 37.15 18.00 18.30	26.70 37.15 18.00 18.30	7.70 4.60 2.50 4.05	15.40 9.20 5.05 8.10	10.25 6.15 3.35 5.40	20.50 12.30 6.75 10.80
	24′	14.4	Solid Brick Solid CM Units Hollow CM Units Brick & Hollow CMU	23.70 33.80 15.45 15.40	24.70 34.80 16.40 16.50	25.75 35.80 17.40 17.65	25.75 35.80 17.40 17.65	25.75 35.80 16.05 15.25	7.70 4.60 2.50 4.05	15.40 9.20 5.05 8.10	10.25 6.15 3.35 5.40	20.50 12.30 6.75 10.80

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CONCRETE ADMIXTURES & SL 🔤 AGGREGATE	03240 Fibrous Reinforcing	Crew	Daily Output	Labor Hours	Unit	Bare Mat.	Bare Labor	Bare Equip.	Bare 🛓
CEMENT	EIRBOUS BEINFORCING	38	S	-	28 - S		28		<u> </u>
CRIBBING	1.1/2 h per CY				CY.	6			
CUTTING	Steel fibers, add to concrete				1.6	44			
DAMPPROOFING	25 lb per CY				CY.	11			
EQUIPMENT	50 lb per CY				CY.	22			
LIFT SLAB	75 lb per CY				CY.	34			
SAWING CONCRETE	100 lb per C Y				CY	44			
WATERPROOFING AND DAMP	100 Cast-In-Place Concrete				0.1.				
WINTER PROTECTION		1							
einforcement	UJJIU Structural Concrete				CV.	72.50			
	2000				C.T.	75.50			
ral Concrete					L.T.	79.90			
	2000 ani				CV.	77 50			
CONCRETE BEADY MIX	2000 psi	1.2			C.T.	77.00			
CONCRETE IN PLACE	2000 psi				CV.	01			
INSULATING CONCRETE	2500 psi				CV.	07			
PLACING CONCRETE	4000 psi				CY	94		_	
te Finishing	4500 psi	10			C.T.	86	· · · · ·		
lly Placed Concrete	5000 psi				CY	90			
te Curing	6000 psi				CY	103			1
ncrete	8000 psi				CY	167			1
us Decks & Underlayments					CY	238			2
	12,000 psi				CY	287			2
estoration & Cleaning	For high early strength cement, add				C.Y.	10.0%			
	For structural lightweight with regular sand, add				C.Y.	25.0%			-
	For all lightweight aggregate, add				C.Y.	45.0%			=
	For integral colors, 2500 psi, 5 bag mix								Ť
	4	1			•	1	I I		` ▶
Settings Estimator Unit Costs As	sembly Costs Project Costs Square Foot Models Residential Models								
03 310 220 0300 Structural concret	te, ready mix, normal weight, 4000 PSI, includes material only								
Qty 1.000 To List Crew	Output Hours Unit C.Y.								
Material 84 Labor	Equip. Total 84 0&P 92.50								

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3 Concrete



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2005 National Average Costs

• B 03100 Concrete Forms & Accessories

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equirements 🛛 🔼	03110 Structural C.I.P. Forms							Daily Output	Labor Hours	Unit	Bare Mat.	Bare Labor	Bare Equip.	Bare Total	Total In 0&P
asio Concrete Mate	FORMS IN PLA	CE, WALLS													
asic concrete Mate	Corbel or haunch	, to 12" wide, a	idd to wall forms, 1 (use			C2	150	.320	L.F.	2.06	10.65		12.71	18.
In Structural CLP 1	2 use						C2	170	.282	L.F.	1.13	9.40		10.53	15.
D3110300 EVPANS	3 use						C2	175	.274	L.F.	.83	9.15		9.98	15.
03110405 EOBMS	4 use						C2	180	.267	L.F.	.67	8.90		9.57	14.
0311040310HM3	Wall, below grade	e, job-built plyw	ood, to 8' high, 1 us	e			C2	300	.160	SFCA	2.37	5.35		7.72	10.
03110415 FORMS	2 use						C2	365	.132	SFCA	1.50	4.38		5.88	8.
03110470 FORMS	3 use						C2	425	.113	SFCA	1.09	3.76		4.85	7.
0311042010HM3	4 use						C2	435	.110	SFCA	.88	3.68		4.56	6.
03110420 FORMS	Over 8' to 16' h	high, 1 use					C2	280	.171	SFCA	4.51	5.70		10.21	13.
02110425 EODMS	2 use						C2	345	.139	SFCA	1.89	4.64		6.53	9.
02110433 FORMS	3 use						C2	375	.128	SFCA	1.57	4.27		5.84	8.
021104461 01M3	4 use						C2	395	.122	SFCA	1.40	4.05		5.45	7.
02110440 FORMS	Exterior wall, 8' t	to 16' high, 1 u	e				C2	280	.171	SFCA	2.18	5.70		7.88	11.
12110456 FORMS	2 use						C2	345	.139	SFCA	1.20	4.64		5.84	8.
02110460 EOPMS	3 use						C2	375	.128	SFCA	.85	4.27		5.12	7.
03110500 GAS ST/	4 use						C2	395	.122	SFCA	.70	4.05		4.75	7.
03110750 BEGLET	Over 16' high,	1 use					C2	235	.204	SFCA	2.40	6.80		9.20	13.
03110200 SCAFED	2 use						C2	290	.166	SFCA	1.32	5.50		6.82	10.
03110000 SCALL	3 use						C2	315	.152	SFCA	.96	5.10		6.06	8.
50 Coporate Access	4 use						C2	330	.145	SFCA	.78	4.85		5.63	8.
onorate Deinforcer	For architectur	al finish, add					C2	1,825	.026	SFCA	5.40	.88		6.28	7.
ast-In-Place Concre	Radial, smooth o	curved, job-bui	t plywood, 1 use				C2	245	.196	SFCA	2.48	6.55		9.03	12.
recent Concrete	2 use						C2	300	.160	SFCA	1.36	5.35		6.71	9.
ementitious Decks	3 use						C2	325	.148	SFCA	.99	4.92		5.91	8.
route	4 use						C2	335	.143	SFCA	.81	4.78		5.59	8_
oncrete Restoration	Below grade, jot	b-built plywood	1 use				C2	225	.213	SFCA	2.99	7.10		10.09	14_
	2 use						51	225	213	SECA	1 65	l 7 10		8 75	12 ≛
Settings Estimator	Unit Costs Assemb	oly Costs Proje	ct Costs Square F	oot Moo	lels][Reside	ential Models	J								
03 110 455 2550 C.	.P. concrete forms,	wall, job built, p	lywood, exterior, 8 t	o 16' hig	ıh, 4 use, in	icludes erect	ing, bracing, s	tripping and	l cleaning					_	
Qty 1.000 T	o List Crew C2	Outp	ut 395	Hours	.122	Unit	SFCA		Antoniniou P						
Material .70	Labor 4.0	15 Equi		Total	4.75		7.05	_							
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B 03200 Concrete Reinforcement



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3 Concrete

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2005 National Average Costs

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lequirements	03210 Reinforcing Steel	Crew	Daily Output	Labor Hours	Unit	Bare Mat.	Bare Labor	Bare Equip.	Bare 🛋
Contra Constante Materiale & Mathew	REINFORCING IN PLACE A615 Grade 60, incl. access. labor	U,							
Casic Concrete Materials & Method	Spirals, hot rolled, 8" to 15" diameter	4 Rodm	2.20	14.545	Ton	1,125	550		1,6
Concrete Points & Accessories	15" to 24" diameter	4 Rodm	2.20	14.545	Ton	1,075	550		1,6;
10 Deinfereine Cheel	24" to 36" diameter	4 Rodm	2.30	13.913	Ton	1,025	530		1,5
	36" to 48" diameter	4 Rodm	2.40	13.333	Ton	970	505		1,4
03210100 ACCESSURIES	48" to 64" diameter	4 Rodm	2.50	12.800	Ton	1,075	485		1,5
03210200 COATED REINFORCI	64" to 84" diameter	4 Rodm	2.60	12.308	Ton	1,125	465		1,5
03210600 REINFORCING IN FD	84" to 96" diameter	4 Rodm	2.70	11.852	Ton	1,175	450		1,6;
20 Wolded Wire Estric	Elevated slabs, #4 to #7	4 Rodm	2.90	11.034	Ton	850	420		1,2
20 Skessing Tenders	Footings, #4 to #7	4 Rodm	2.10	15.238	Ton	760	580		1,3
40 Eibreus Beinfereing	Footings, #4 to #7	4 Rodm	4,200	.008	Lb.	.42	.29		
Au Fibrous Reinfording	#8 to #18	4 Rodm	3.60	8.889	Ton	720	335		1,0
Cast-In-Flace Concrete	#8 to #18	4 Rodm	7,200	.004	Lb.	.42	.17		
Frecast Concrete	Slab on grade, #3 to #7	4 Rodm	2.30	13.913	Ton	760	530		1,2
Servite	Slab on grade, #3 to #7	4 Rodm	4,200	.008	Lb.	.40	.29		
Concrete Restoration & Cleaning	Walls, #3 to #7	4 Rodm	3	10.667	Ton	760	405		
concrete mestoration & cleaning	#8 to #18	4 Rodm	4	8	Ton	760	305		1,0
	Use the following for a rough estimate guide								
d Plastice	Typical in place, average, under 10 ton job, #3 to #7	4 Rodm	1.80	17.778	Ton	825	675		1,5
nd Moisture Protection	#8 to #18	4 Rodm	2.70	11.852	Ton	845	450		1,2
1) Vindowa	10 - 50 ton job, #3 to #7	4 Rodm	2.10	15.238	Ton	810	580		1,3
	#8 to #18	4 Rodm	3	10.667	Ton	830	405		1,2
	50 - 100 ton job, #3 - #7	4 Rodm	2.20	14.545	Ton	790	550		1,3
es t	#8 to #18	4 Rodm	3.10	10.323	Ton	810	390		1,2
	Over 100 ton job, #3 - #7	4 Rodm	2.30	13.913	Ton	785	530		1,3
lgs Construction	#8 - #18	4 Rodm	3.20	10	Ton	800	380		1,1
ng Sustems	High strength steel, Grade 75, #14 bars only, add				Ton	60			Ē
	Unloading & sorting, add to above	C5	100	560	Ton		20,50	6 15	<u> </u>
Settings Estimator Unit Costs As	sembly Costs [Project Costs] [Square Foot Models] [Residential Models]								
03 210 600 0700 Reinforcing steel,	in place, walls, #3 to #7, A615, grade 60, incl access. Labor								
Qty 1.000 To List Crew	4 Rodm Output 3 Hours 10.667 Unit Ton								
Material 760 Labor	405 Equip. Total 1,165 0&P 1,500								
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4 Masonry

2005 National Average Costs • B 04800 Masonry Assemblies

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ssemblies 🛛 🖾 BRICK	04810 Unit Masonry Assemblies	Crew	Daily Output	Labor Hours	Unit	Bare Mat.	Bare Labor	Bare Equip	Bare 🛓
LAVED AERATED CONCRETE F		14.28	output	Tiodro	8 5		2	E quip.	
VENEER	CUNCRETE BLUCK, DECURATIVE C90, 2000 psi		-	-	2	2.2.2.2			
SIZED BRICK	For bullnose block, add		·			10.0%	·		
EY _	For special color, add		1			13.0%	-		
EX BLOCK	CONCRETE BLOCK, EXTERIOR C90, 2000 psi		·		· ·				
INS	Reinforced alt courses, tooled joints 2 sides								
	Normal weight, 8" x 16" x 6" thick	D8	395	.101	S.F.	1.67	3.23		
RETE BLOCK BOND BEAM	8" thick	D8	360	.111	S.F.	2.48	3.55		
	10" thick	D8	290	.138	S.F.	3	4.40		
	12" thick	D9	250	.192	S.F.	3.01	5.95		
STE BLOCK, DECORATIVE	Lightweight, 8" x 16" x 6" thick	D8	450	.089	S.F.	1.96	2.84		
RETE BLUCK, EXTERIOR	8" thick	D8	430	.093	S.F.	2.65	2.97		
RETE BLUCK FUUNDATION WAI	10" thick	D8	395	101	SE	2.99	3.23		
RETE BLOCK, HIGH STRENGTH	12" thick	D9	350	137	SE	4.31	4.26		
RETE BLOCK INSULATION INSE	CONCRETE BLOCK FOUNDATION WALL C90/C145		000		0.1.	1.01	1.20		
RETE BLOCK, INTERLOCKING	Normal-weight, cut joints, horiz joint reinf, no vert reinf								
RETE BLOCK, LINTELS	Hollow O' v 1C' v C' Ibiol	DO	455	000	CE	1.67	2.01		
RETE BLOCK, PARTITIONS		00	400	.000	5.F.	1.07	2.01		
RETE BRICK		00	420	.034	э.г. с.г.	1.00	3 2 65		
RETE SCREEN BLOCK		D0	300	.114	э.г.	2.43	3.60		
G		DS	300	.160	S.F.	2.01	4.97		
G PANELS	Solid, 8" x 16" block, 6" thick	08	440	.091	5.F.	1.81	2.90		
BLOCK	8" thick	D8	415	.096	S.F.	2.59	3.08		
D CONCRETE BLOCK	12" thick	D9	350	.137	S.F.	3.76	4.26		
COTTA	CONCRETE BLOCK, HIGH STRENGTH Normal weight		·						
	Hollow, reinforced alternate courses, 8" x 16" units	-	-				-)		
	3500 psi, 4" thick	D8	440	.091	S.F.	1.24	2.90		
	6" thick	D8	395	.101	S.F.	1.64	3.23		
	8" thick	D8	360	.111	S.F.	2.44	3.55		Ŧ
¥	12" thick	D9	250	192	SE	2.96	5.95		_
< >									•
Settings Estimator Unit Costs A	ssembly Costs Project Costs Square Foot Models Residential Models								
04 810 186 0350 Concrete mason	ry unit (CMU), foundation wall, trowel cut joints, normal weight, hollow, 2000 psi, 12'' x 8	" x 16", include	es mortar ar	nd horizont	al joint re	einforcing eve	ery other		10
Qty 1.000 To List Crew	D9 Output 300 Hours .160 Unit S.F.								
Material 2.51 Labor	4.97 Equip. Total 7.48 0&P 10.35	_							
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Crews

Crew No.	Bare	Costs	In Subs	ici. O & P	Cost Per Labor-Hour			
Crew B-95A	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P		
1 Equip. Oper. (crane)	\$35.90	\$287.20	\$54.10	\$432.80	\$31.30	\$47.83		
1 Laborer	26.70	213.60	41.55	332.40				
1 Hyd. Excavator, 5/8 C.Y.		432.40		475.65	27.03	29.73		
16 L.H., Daily Totals		\$933.20		\$1240.85	\$58.33	\$77.56		
Crew B-95B	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P		
1 Equip. Oper. (crane)	\$35.90	\$287.20	\$54.10	\$432.80	\$31.30	\$47.83		
1 Laborer	26.70	213.60	41.55	332.40	45.02	40.50		
1 Hyd. Excavator, 1.5 c.t.		¢120.40		(1557.65	43.05	49.00		
10 L.H., Vally IOLais		\$1221.20		\$1357.05	\$/0.55 Dama	397.30		
Crew B-95C	Hr.	Daily	Hr.	Daily	Costs	O&P		
1 Fouin. Oper. (crane)	\$35.90	\$287,20	\$54.10	\$432,80	\$31.30	\$47.83		
1 Laborer	26.70	213.60	41.55	332.40		*		
1 Hyd. Excavator, 2.5 C.Y.		1215.00		1336.50	75.94	83.53		
16 L.H., Daily Totals		\$1715.80		\$2101.70	\$107.24	\$131.36		
Crew C-1	Hr.	Daily	Hr.	Daily	Bare	Incl.		
2 Camontars	\$34.25	\$822.00	\$53.35	\$1280.40	\$32.36	\$50.40		
1 Laborer	26.70	213.60	41.55	332.40	002.00	900.40		
32 L.H., Daily Totals		\$1035.60		\$1612.80	\$32.36	\$50.40		
					Bare	Incl.		
Crew C-2	Hr.	Daily	Hr.	Daily	Costs	O&P		
1 Carpenter Foreman (out)	\$36.25	\$290.00	\$56.45	\$451.60	\$33.33	\$51.90		
4 Carpenters	34.25	1096.00	53.35	1707.20				
1 Laborer	26.70	213.60	41.55	332.40				
48 L.H., Daily Totals		\$1599.60		\$2491.20	\$33.33	\$51.90		
Crew C-2A	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P		
1 Carpenter Foreman (out)	\$36.25	\$290.00	\$56.45	\$451.60	\$33.09	\$51.01		
3 Carpenters	34.25	822.00	53.35	1280.40				
1 Cement Finisher	32.80	202.00	48.55	380.60				
481 H. Daily Totals	20.10	\$1588,40	41.00	\$2451.20	\$33.09	\$51.01		
to carry oddy rotate		¥1000.10		VETUILEU	Rare	Incl		
Crew C-3	Hr.	Daily	Hr.	Daily	Costs	O&P		
1 Rodman Foreman	\$39.95	\$319.60	\$65.90	\$527.20	\$34.78	\$56.15		
4 Rodmen (reinf.)	37.95	1214.40	62.60	2003.20				
1 Equip. Oper. (light)	33.05	264.40	49.80	398.40				
3 Stressing Equipment	20.10	40.80	41.00	44.90				
.5 Grouting Equipment		76.40		84.05	1.83	2.01		
64 L.H., Daily Totals		\$2342.80		\$3722.55	\$36.61	\$58.16		
Crow C 4	Ur.	Daily	Ur.	Daily	Bare	Incl.		
L Dodmon Foreman	HI.	\$210.60	HI.	0ally	COSIS	0&P		
2 Rodman Foreinan 2 Rodman (reinf.)	37.95	010.80	500.90	5527.20	Q38.40	\$03.45		
3 Stressing Equipment	31.50	40.80	02.00	44.90	1.28	1.40		
32 L.H., Daily Totals		\$1271.20		\$2074.50	\$39.73	\$64.83		
				_	Bare	Inci.		
Crew C-5	Hr.	Daily	Hr.	Daily	Costs	O&P		
1 Rodman Foreman	\$39.95	\$319.60	\$65.90	\$527.20	\$36.82	\$59.39		
4 Rodmen (reint.)	37.90	297.20	62.60	2003.20				
1 Equip. Oper. (crane) 1 Equip. Oper. (iler	30.10	240,80	45.35	362.80				
1 Hyd. Crane, 25 Ton		616.80		678.50	11.01	12.12		
56 L.H., Daily Totals		\$2678.80		\$4004.50	\$47.83	\$71.51		

Crew No.	Bare	Costs	lne Subs (ы. О&Р	Cost Per Labor-Hour		
Crew C-6	Hr.	Daily	Hr.	Daily	Bare Costs	Inci. 0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.06	\$43.15	
4 Laborers	26.70	854.40	41.55	1329.60			
1 Cement Finisher	32.85	262.80	48.35	386.80	1.00		
2 Gas Engine Worators		48.00		52.80	1.00	1.10	
40 L.H., Daily IOLais		\$1394,00		Ş2120.00	\$29.00 Dava		
Crew C-7	Hr.	Daily	Hr.	Daily	Costs	Inci. 0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.87	\$44.22	
3 Laborers 1 Cement Finisher	32.85	262.80	41.35	386.80			
1 Equip. Oper. (med.)	34.65	277.20	52.20	417.60			
1 Equip. Oper. (oiler)	30.10	240.80	45.35	362.80			
2 Gas Engine Vibrators		48.00		52.80			
1 Concrete Bucket, 1 C.Y.		16.00		17.60	12.22	14.65	
72 L H. Daily Totak		\$3037.80		904.90 \$424215	\$42.20	\$58.88	
72 E.H., Daily lotals		<i>30037100</i>		J4242.13	Rare	Incl	
Crew C-7A	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$27.16	\$42.06	
5 Laborers	26.70	1068.00	41.55	1662.00			
2 Truck Drivers(Heavy) 2 Conc. Transit Mixers	27.55	440.80	42.00	6/2.00	2314	25.45	
64 L.H., Daily Totals		\$3219.20		\$4320.50	\$50.30	\$67.51	
					Bare	Incl.	
Crew C-7B	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.53	\$43.99	
5 Laborers	26.70	1068.00	41.55	1662.00			
1 Equipment Operator (neavy) 1 Equipment Oiler	30.10	287.20	04.10 45.35	432.80			
1 Conc. Bucket, 2 C.Y.	50.10	24.60	40.00	27.05			
1 Truck Crane, 165 Ton		1912.00		2103.20	30.26	33.29	
64 L.H., Daily Totals		\$3762.20		\$4945.45	\$58.79	\$77.28	
Crew C-7C	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.94	\$44.61	
5 Laborers	26.70	1068.00	41.55	1662.00			
2 Equipment Operator (medium)	34.65	554.40	52.20	835.20	10.00	15.00	
2 Wheel Loader, 4 C.Y.		891.20		980.30	13.93	15.32	
04 L.H., Daily IOlais		\$2/43.20		22022710	942.07	209.95	
Crew C-7D	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.12	\$43.52	
5 Laborers	26.70	1068.00	41.55	1662.00			
1 Equipment Operator (med.)	34.00	277.20	52.20	417.00	2 73	3.00	
56 L.H., Daily Totals		\$1727.60		\$2605.30	\$30.85	\$46.52	
					Bare	Incl.	
Crew C-8	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$29.88	\$45.36	
3 Laborers 2 Coment Finishers	20.70	640.80 525.60	41.55	997.20 773.60			
1 Equip. Oper. (med.)	34.65	277.20	52,20	417.60			
1 Concrete Pump (small)		704.20		774.60	12.58	13.83	
56 L.H., Daily Totals		\$2377.40		\$3320.60	\$42.46	\$59.19	
Crow C.84	Lip-	Daily	LL.	Daily	Bare	Inci.	
1 Lahor Foreman (outsida)	\$28.70	\$220.60	\$44.70	\$357.60	\$20.08	\$44.23	
3 Laborers	26.70	640.80	41.55	997.20	J23.00	Q44.23	
2 Cement Finishers	32.85	525.60	48.35	773.60			
48 L.H., Daily Totals		\$1396.00		\$2128.40	\$29.08	\$44.23	

Crews

Crew No.	Bare	Costs	lr Subs	o & P	Cost Per Labor-Hour		
Crew C-14D	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P	
1 Carpenter Foreman (out)	\$36.25	\$290.00	\$56.45	\$451.60	\$33.98	\$53.01	
18 Carpenters	34.25	4932.00	53.35	7682.40	1.0.0000000000		
2 Rodmen (reinf.)	37.95	607.20	62.60	1001.60			
2 Laborers	26.70	427.20	41.55	664.80			
1 Cement Finisher	32.85	262.80	48.35	386.80			
1 Equip. Oper. (med.)	34.65	277.20	52.20	417.60			
1 Gas Engine Vibrator		24.00		26.40			
1 Concrete Pump (small)		704.20		774.60	3.64	4.01	
200 L.H., Daily Totals		\$7524.60		\$11405.80	\$37.62	\$57.02	
Crow C-14E	Hr	Daily	H۲	Daily	Bare	Incl.	
1 Camenter Foreman (out)	\$36.25	\$290.00	\$56.45	\$451.60	\$23.50	\$53.20	
2 Camenters	34.25	548.00	53 35	853.60	335.55	000.20	
A Rodmen (reinf)	37.95	1214 40	62.60	2003.20			
3 Lahovers	26.70	640.80	41.55	997.20			
1 Cement Finisher	32.85	262.80	48.35	386.80			
1 Gas Engine Vibrator	02.00	24.00	10.00	26.40	.27	.30	
88 L.H., Daily Totals		\$2980.00		\$4718.80	\$33.86	\$53.59	
					Bare	Incl.	
Crew C-14F	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Laborer Foreman (out)	\$28.70	\$229.60	\$44.70	\$357.60	\$31.02	\$46.20	
2 Laborers	26.70	427.20	41.55	664.80			
6 Cement Finishers	32.85	1576.80	48.35	2320.80			
1 Gas Engine Vibrator		24.00		26.40	.33	.37	
72 L.H., Daily Totals		\$2257.60		\$3369.60	\$31.35	\$46.57	
	10	101000	12	10/15/201	Bare	Incl.	
Crew C-14G	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Laborer Foreman (out)	\$28.70	\$229.60	\$44.70	\$357.60	\$30.50	\$45.69	
2 Laborers	26.70	427.20	41.55	664.80			
4 Cement Finishers	32.85	1051.20	48.35	1547.20			
1 Gas Engine Vibrator		24.00		26.40	.43	.47	
56 L.H., Daily Totals		\$1732.00		\$2596.00	\$30.93	\$46.16	
Crew C-14H	Hr.	Daily	Hr.	Dailv	Bare Costs	Incl. O&P	
1 Carpenter Foreman (out)	\$36.25	\$290.00	\$56.45	\$451.60	\$33.71	\$52.55	
2 Carpenters	34.25	548.00	53.35	853.60			
1 Rodman (reinf.)	37.95	303.60	62.60	500.80			
1 Laborer	26.70	213.60	41.55	332.40			
1 Cement Finisher	32.85	262.80	48.35	386.80			
1 Gas Engine Vibrator		24.00		26.40	.50	.55	
48 L.H., Daily Totals		\$1642.00		\$2551.60	\$34.21	\$53.10	
Crew C-15	Hr	Daily	Hr.	Dailv	Bare Costs	Incl. O&P	
1 Carpenter Foreman /outi	\$36.25	\$290.00	\$56.45	\$451.60	\$32.06	\$49.60	
2 Carpenters	34.25	548.00	53.35	853.60		<i>v</i> 10.00	
3 Laborers	26.70	640.80	41.55	997.20			
2 Cement Finishers	32.85	525.60	48.35	773.60			
1 Rodman (reinf.)	37.95	303.60	62.60	500.80			
72 L.H., Daily Totals		\$2308.00		\$3576.80	\$32.06	\$49.60	
		22.2222			Bare	Incl.	
Crew C-16	Hr.	Daily	Hr.	Daily	Costs	0&P	
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$31.67	\$49.19	
3 Laborers	26.70	640.80	41.55	997.20			
2 Cement Finishers	32.85	525.60	48.35	773.60			
1 Equip. Oper. (med.)	34.65	277.20	52.20	417.60			
2 Rodmen (reinf.)	37.95	607.20	62.60	1001.60	0.70	10.70	
1 Concrete Pump (small)		/04.20		//4.60	9.78	10.76	
72 L.H., Daily lotals		\$2984.60		\$4322.20	\$41.45	\$59.95	

Crew No.	Bare	Costs	lne Subs (ci. O & P	Cost Per Labor-Hour			
Come 0 17	11.	Daily	11-	Dailu	Bare	Incl.		
2 Skilled Worker Foremen	536.85	\$589.60	ні. \$57.30	\$916.80	\$35,25	\$54.82		
8 Skilled Workers	34.85	2230.40	54.20	3468.80	000.20	001.02		
80 L.H., Daily Totals		\$2820.00		\$4385.60	\$35.25	\$54.82		
Crew C-17A	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P		
2 Skilled Worker Foremen	\$36.85	\$589.60	\$57.30	\$916.80	\$35.26	\$54.81		
8 Skilled Workers	34.85	2230.40	54.20	3468.80				
.125 Equip. Oper. (crane) .125 Crane, 80 Ton, & Tools	30.90	35.90	54.10	54.10 136.80	1.54	1.69		
81 L.H., Daily Totals		\$2980.28		\$4576.50	\$36.80	\$56.50		
0					Bare	Incl.		
2 Skilled Worker Foremen	Hr. \$26.95	SERD ED	Hr. ¢57.20	Cole PO	Costs	0&P		
2 Skilled Workers	34.85	2230.40	54.20	3468.80	930.ZT	QJ4.00		
.25 Equip. Oper. (crane)	35.90	71.80	54.10	108.20				
.25 Crane, 80 Ton, & Tools 25 Walk Debind Power Tools		248.75		273.65	211	2.42		
82 L.H., Daily Totals		\$3146.70		\$4774.20	\$38.38	\$58.22		
					Bare	Incl.		
Crew C-17C	Hr.	Daily	Hr.	Daily	Costs	0&P		
2 Skilled Worker Foremen 8 Skilled Workers	\$36.85	\$589.60	\$57.30	\$916.80	\$35.27	\$54.79		
.375 Equip. Oper. (crane)	35.90	2230.40	54.20	162.30				
.375 Crane, 80 Ton & Tools	00000.00	373.13	1.000-0.01	410.45	4.50	4.95		
83 L.H., Daily Totals		\$3300.83		\$4958.35	\$39.77	\$59.74		
Crew C-17D	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P		
2 Skilled Worker Foremen	\$36.85	\$589.60	\$57.30	\$916.80	\$35.28	\$54.79		
8 Skilled Workers 5 Equip. Oper. (crane)	34.85	2230.40	54.20 54.10	3468.80				
.5 Crane, 80 Ton & Tools	33.50	497.50	34.10	547.25	5.92	6.51		
84 L.H., Daily Totals		\$3461.10		\$5149.25	\$41.20	\$61.30		
Crew C-17E	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P		
2 Skilled Worker Foremen	\$36.85	\$589.60	\$57.30	\$916.80	\$35.25	\$54.82		
8 Skilled Workers	34.85	2230.40	54.20	3468.80		1.00		
80 L.H., Daily Totals	-	\$2899.00		\$4472.50	536.24	\$55.91		
					Bare	Inci.		
Crew C-18	Hr. \$29.70	\$29.70	HT. \$44.70	SAA 70	Costs	0&P \$41.00		
1 Laborer	26.70	213.60	41.55	332.40	.JZ0.92	Q41.90		
1 Concrete Cart, 10 C.F.		49.80		54.80	5.53	6.09		
9 L.H., Daily Totals		\$292.10		\$431.90	\$32.45	\$47.99		
Crew C-19	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P		
.125 Labor Foreman (out)	\$28.70	\$28.70	\$44.70	\$44.70	\$26.92	\$41.90		
1 Laborer 1 Concrete Cart 18 C.F.	26.70	213.60 76.80	41.55	332.40 84.50	8.53	9.39		
9 L.H., Daily Totals		\$319.10		\$461.60	\$35.45	\$51.29		
1447 - 10494A					Bare	Incl.		
Crew C-20	Hr.	Daily	Hr.	Daily	Costs	0&P		
1 Labor Foreman (outside) 5 Laborers	\$28.70	\$229.60	\$44.70	\$357.60	\$28.71	\$44.08		
1 Cement Finisher	32.85	262.80	48.35	386.80				
1 Equip. Oper. (med.)	34.65	277.20	52.20	417.60				
2 Gas Engine Vibrators 1 Concrete Pump (creal)		48.00		52.80 774.60	11.75	12.02		
64 L.H., Daily Totals		\$2589.80		\$3651.40	\$40.46	\$57.01		

Crews

Crew No.	Bare	Costs	ln Subs	o & P	Co Per Lab	st or-Hour		Crew No.	lo. Bare Cos		Incl. Subs O & P		Cost Per Labor-Hour	
Crew C-21	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P		Crew D-2		Daily	Hr.	Daily	Bare Costs	Inci. 0&P
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$28.71	\$44.08		3 Bricklayers	\$35.25	\$846.00	\$53.70	\$1288.80	\$32.12	\$49.05
5 Laborers	26.70	1068.00	41.55	1662.00				2 Bricklayer Helpers	26.90	430.40	41.00	656.00		
1 Cement Finisher	32.85	262.80	48.35	386.80				.5 Carpenter	34.25	137.00	53.35	213.40		
1 Equip. Oper. (med.) 2 Cap Engine Wheetern	34.65	2//.20	52.20	417.60				44 L.H., Daily Totals		\$1413.40		\$2158.20	\$32.12	\$49.05
2 Gas Eligne violators 1 Concrete Conveyer		48.00		52.80 168.10	314	3.45							Bare	Incl.
641.H. Daily Totals		\$2038.40		\$3044.90	\$31.85	\$47.53		Crew D-3	Hr.	Daily	Hr.	Daily	Costs	0&P
		,			Rare	Incl		3 Bricklayers	\$35.25	\$846.00	\$53./0	\$1288.80	\$32.02	\$48.85
Crew C-22	Hr.	Daily	Hr.	Daily	Costs	O&P		2 bricklayer helpers 25 Camenter	20.90	430.40	53.35	106.70		
1 Rodman Foreman	\$39.95	\$319.60	\$65.90	\$527.20	\$38.10	\$62.62		42 L.H., Daily Totals	01.20	\$1344.90	00.00	\$2051.50	\$32.02	\$48.85
4 Rodmen (reinf.)	37.95	1214.40	62.60	2003.20				ie eini, oaij ioan		Q.CT.IDC		42001.00	Rare	Incl
.125 Equip. Oper. (crane)	35.90	35.90	54.10	54.10				Crew D-4	Hr.	Daily	Hr.	Daily	Costs	0&P
.125 Equip. Oper. Oiler	30.10	30.10	45.35	45.35				1 Bricklaver	\$35.25	\$282.00	\$53.70	\$429.60	\$30.53	\$46.38
.125 Hyd. Crane, 25 Ton		77.10		84.80	1.84	2.02		2 Bricklayer Helpers	26.90	430.40	41.00	656.00		
42 L.H., Daily lotals		\$16//.10		\$2/14.65	\$39.94	\$64.64		1 Equip. Oper. (light)	33.05	264.40	49.80	398.40		
0		D-II.		Della	Bare	Incl.		1 Grout Pump, 50 C.F./hr		107.75		118.55		
Crew C-23	Hr.	Daily	Hr.	Daily	Costs	U&P		1 Hoses & Hopper		15.20		16.70		
2 Skilled Worker Foremen 6 Skilled Workers	\$36.85	\$589.60 1672.80	\$57.30	\$916.80	\$34.88	\$53.93		1 Accessories		11.90		13.10	4.22	4.64
1 Equin Oner (grane)	35.90	287.20	54.20	432.80				32 L.H., Daily lotals		\$1111.65	<u> </u>	\$1632.35	\$34.75	\$51.02
1 Equip. Oper. Oiler	30.10	240.80	45.35	362.80				Crow D E	LI-	Daily		Daily	Bare	Inci.
1 Crane, 90 Ton		1325.00		1457.50	16.56	18.22		1 Drieldouer	COE 05	Capa on	ni. 650.70	C 400 60	60515	00F
80 L.H., Daily Totals		\$4115.40		\$5771.50	\$51.44	\$72.15		1 Brichayer	\$39.29	\$282.00	\$53.70	\$429.60	\$30.20	\$53.70
					Bare	Inci.		o L.n., Dally Nuals		\$262.00	<u> </u>	\$429.00	\$30.29	\$35.70
Crew C-23A	Hr.	Daily	Hr.	Daily	Costs	O&P		Crew D-6	Hr	Daily	Hr	Daily	Bare	Inci.
1 Labor Foreman (outside)	\$28.70	\$229.60	\$44.70	\$357.60	\$29.62	\$45.45		2 Drieldoware	¢25.25	\$946.00	¢52.70	\$1.200.00	\$21.20	\$47.50
2 Laborers	26.70	427.20	41.55	664.80				3 Bricklaver Helpers	26.90	645.60	41.00	984.00	\$51.20	947.05
1 Equip. Oper. (crane)	35.90	287.20	54.10	432.80				.25 Carpenter	34.25	68.50	53.35	106.70		
1 Equip. Oper. Oiler	30.10	240.80	45.35	362.80				50 L.H., Daily Totals		\$1560.10		\$2379.50	\$31.20	\$47.59
3 Coorc bucket & C.Y		465.60		51215	49.62	54 58							Bare	Incl.
40 L.H., Daily Totals		\$3169.40		\$4001.05	\$79.24	\$100.03		Crew D-7	Hr.	Daily	Hr.	Daily	Costs	0&P
					Rare	Incl		1 Tile Layer	\$32.70	\$261.60	\$48.05	\$384.40	\$29.03	\$42.65
Crew C-24	Hr.	Daily	Hr.	Daily	Costs	O&P		1 Tile Layer Helper	25.35	202.80	37.25	298.00		
2 Skilled Worker Foremen	\$36.85	\$589.60	\$57.30	\$916.80	\$34.88	\$53.93		16 L.H., Daily Totals		\$464.40		\$682.40	\$29.03	\$42.65
6 Skilled Workers	34.85	1672.80	54.20	2601.60			[Bare	Inci.
1 Equip. Oper. (crane)	35.90	287.20	54.10	432.80				Crew D-8	Hr.	Daily	Hr.	Daily	Costs	0&P
1 Equip. Oper. Oiler	30.10	240.80	45.35	362.80				3 Bricklayers	\$35.25	\$846.00	\$53.70	\$1288.80	\$31.91	\$48.62
1 Truck Crane, 150 Ton	-	1445.00		1589.50	18.06	19.87		2 Bricklayer Helpers	26.90	430.40	41.00	656.00	A	A 40. 00
80 L.H., Daily lotais		\$4235.40		\$5903.50	\$52.94	\$/3.80		40 L.H., Daily lotals	_	\$12/6.40		\$1944.80	\$31.91	\$48.62
Crew C-25	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P		Crew D-9	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P
2 Rodmen (reinf.)	\$37.95	\$607.20	\$62.60	\$1001.60	\$29.78	\$49.70		3 Bricklayers	\$35.25	\$846.00	\$53.70	\$1288.80	\$31.08	\$47.35
2 Rodmen Helpers	21.60	345.60	36.80	588.80			L	3 Bricklayer Helpers	26.90	645.60	41.00	984.00		
32 L.H., Daily Totals		\$952.80		\$1590.40	\$29.78	\$49.70	[48 L.H., Daily Totals		\$1491.60		\$2272.80	\$31.08	\$47.35
Crew C-27	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. O&P	[Crew D-10	Hr.	Daily	Hr.	Daily	Bare Costs	Incl. 0&P
2 Cement Finishers	\$32.85	\$525.60	\$48.35	\$773.60	\$32.85	\$48.00		1 Bricklayer Foreman	\$37.25	\$298.00	\$56.75	\$454.00	\$32.44	\$49.31
1 Concrete Saw		114.40		125.85	7.15	7.87		1 Bricklayer	35.25	282.00	53.70	429.60		
16 L.H., Daily Totals		\$640.00		\$899.45	\$40.00	\$55.87		2 Bricklayer Helpers	26.90	430.40	41.00	656.00		
100 - M204440					Bare	Inci.		1 Equip. Oper. (crane)	35.90	287.20	54.10	432.80	10.05	10.01
Crew C-28	Hr.	Daily	Hr.	Daily	Costs	O&P		1 ITUCK CRANE, 12.5 TON		505.80	ļ	556.40	12.65	13.91
1 Cement Finisher	\$32.85	\$262.80	\$48.35	\$386.80	\$32.85	\$48.00		40 L.N., Dally IDEAIS		Ş1803.40		Q2028.80	\$45.09	303.22
1 Portable Air Compressor		17.30		19.05	2.16	2.37		Crow D.11	ц.	Daily	Li.e	Daily	Bare	Incl.
8 L.H., Daily Totals		\$280.10		\$405.85	\$35.01	\$50.37		1 Dricklauge Commen	for 105	\$200.00	ni. 656.75	CASA 00	\$22.12	\$50.49
					Bare	Incl.		1 Bricklaver	35.25	282.00	\$30./5 52.70	\$454.00 429.60	\$33.13	\$30.46
Crew D-1	Hr.	Daily	Hr.	Daily	Costs	O&P		1 Bricklaver Helper	26.90	215.20	41.00	328.00		
1 Bricklayer	\$35.25	\$282.00	\$53.70	\$429.60	\$31.08	\$47.35		24 L.H., Daily Totals	20120	\$795.20	14.00	\$1211.60	\$33.13	\$50.48
1 BIICKWYER HEIDER	20.90	215.20	41.00	328.00	601.00	647.05	°							
to L.H., Daily lotals	1	\$497.20		\$/5/.60	\$31.08	\$47.35								

CREWS



APPENDIX C

Mechanical Breadth

DETAIL REPORT

Marrowski				Esti Proj-	mator: JAM ect Size: 99100 S	QFT	PLUMBING	3 DD 070706		
PA	PLUMBING DD 070706			Deta Gro Gro	ul - With Taxes a up 1: Subdivision up 2: Element	nd Insurance	,Indirect Costs a	re Spread		
Elemer	nt Description	Quantity	UM	Mat.Unit	Mat.Total	MH/Unit	Tot.Hours	Sub.Total	Egp.Total	TotalCost
DOMES 0800 0800 0800 0800 0800 0800 0800 08	IG ESTIMATE TIC WATER SUPPLY ALLOWANCE FOR MECH ROOM DOMESTIC SERVICE ENTRANCE FLANGE PACK,2-1/2* FLANGE PACK,3* FLANGE PACK,4* COPPER PIPE (TUBING)	1.00 1.00 8.00 2.00 2.00	LS EA EACH EACH EACH	13,780.00 2,968.00 6.63 6.89 11.93	13,780.00 2,968.00 53.00 13.78 23.85	200.00 40.00 0.24 0.25 0.36	200.0 40.0 1.9 0.5 0.7			26,451.92 5,523.58 166.27 43.28 66.78
0800 0800 0800 0800 0800 0800 0800 080	TYPE L PIPE,1/2" PIPE,3/4" PIPE,1-1/4" PIPE,1-1/2" PIPE,2" PIPE,2" PIPE,3" PIPE,4" COPPER FITTINGS	2,366.00 2,251.00 875.00 1,214.00 722.00 879.00 681.00 172.00 80.00	LNFT LNFT LNFT LNFT LNFT LNFT LNFT LNFT	1.75 2.70 3.84 5.40 6.96 10.96 16.59 22.26 37.18	4,143.15 6,070.14 3,364.04 6,552.59 5,024.33 9,636.06 11,300.00 3,829.27 2,974.11	0.06 0.08 0.08 0.08 0.09 0.12 0.14 0.18	142.0 135.1 70.0 97.1 57.8 79.1 81.7 24.1 14.4			12,573,89 14,303,93 7,653,32 12,692,18 8,788,44 15,066,97 17,044,69 5,571,98 4,084,68
0800	95/5 SOLDER		****							

PLUMBING ESTIMA

0800	ALLOWANCE FOR MECH ROOM	1.00	LS	13,780.00	13,780.00	200.00	200.0	26,451.92	0.267
0800	DOMESTIC SERVICE ENTRANCE	1.00	EA	2,968.00	2,968.00	40.00	40.0	5,523.58	0.056
0800	FLANGE PACK,2-1/2"	8.00	EACH	6.63	53.00	0.24	1.9	166.27	0.002
0800	FLANGE PACK,3"	2.00	EACH	6.89	13.78	0.25	0.5	43.28	
0800	FLANGE PACK,4*	2.00	EACH	11.93	23.85	0.36	0.7	66.78	0.001
0800	COPPER PIPE (TUBING)								
0800	TYPEL			0.000	0.0710.0210.020	1000	10122-022		
0800	PIPE,1/2"	2,366.00	LNFT	1.75	4,143.15	0.06	142.0	12,573.89	0.127
0800	PIPE,3/4"	2,251.00	LNFT	2.70	6,070.14	0.06	135.1	14,303.93	0.144
0800	PIPE,1"	875.00	LNFT	3.84	3,364.04	0.08	70.0	7,653.32	0.077
0800	PIPE,1-1/4"	1,214.00	LNFT	5.40	6,552.59	0.08	97.1	12,692.18	0.128
0800	PIPE,1-1/2"	722.00	LNFT	6.96	5,024.33	0.08	57.8	8,788.44	0.089
0800	PIPE,2"	879.00	LNFT	10.96	9,636.06	0.09	79.1	15,066.97	0.152
0800	PIPE,2-1/2"	681.00	LNFT	16.59	11,300.00	0.12	81.7	17,044.69	0.172
0800	PIPE,3"	172.00	LNFT	22.26	3,829.27	0.14	24.1	5,571.98	0.056
0800	PIPE,4"	80.00	LNFT	37.18	2,974.11	0.18	14.4	4,084.68	0.041
0800	COPPER FITTINGS		****						
0800	95/5 SOLDER		****						
0800	90 ELL,1/2"	644.00	EACH	0.39	252.24	0.33	211.2	12,205.63	0.123
0800	90 ELL,3/4"	120.00	EACH	0.88	105.35	0.43	51.8	3,043.27	0.031
0800	90 ELL,1*	186.00	EACH	2.16	402.27	0.48	89.3	5,484.10	0.055
0800	90 ELL,1-1/4"	61.00	EACH	3.26	199.03	0.57	34.6	2,175.49	0.022
0800	90 ELL, 1-1/2"	37.00	EACH	5.10	188.57	0.59	21.9	1,444.33	0.015
0800	90 ELL,2"	37.00	EACH	9.27	343.00	0.69	25.5	1,814.79	0.018
0800	90 ELL,2-1/2"	20.00	EACH	19.57	391.32	1.10	21.9	1,668,26	0.017
0800	90 ELL,3"	7.00	EACH	26.14	183.01	1.31	9.2	719.93	0.007
0800	90 ELL,4"	4.00	EACH	66.92	267.70	1.75	7.0	690.21	0.007
0800	TEE,1/2*	54.00	EACH	0.67	35.93	0.47	25.5	1,478.82	0.015
0800	TEE,3/4*	7.00	EACH	1.62	11.31	0.62	4.3	255.94	0.003
0800	_ TEE,1-1/2"	2.00	EACH	11.08	22.17	0.86	1.7	121.97	0.001
0800	REDUCING TEE,3/4"	67.00	EACH	1.55	.104.14	0.55	37.0	2,203.02	0.022
0800	REDUCING TEE,1"	48.00	EACH	5.28	253.42	0.69	33.0	2,143.62	0.022
0800	REDUCING TEE, 1-1/4"	44.00	EACH	9.97	438.64	0.77	33.8	2,390.72	0.024
0800	REDUCING TEE, 1-1/2"	56.00	EACH	16.54	926.43	0.82	45.7	3,599,51	0.036
0800	REDUCING TEE,2"	45.00	EACH	22.47	1.011.16	0.94	42.1	3,490,78	0.035
0800	REDUCING TEE,2-1/2"	23.00	EACH	50.89	1,170,49	1.51	34.8	3,251,33	0.033
0800	REDUCING TEE,3"	8.00	EACH	73.07	584.59	1.84	14.7	1.474.28	0.015



Table 3.2 – Flow Velocity											
Flow Rate				ft/	sec						
GPM	3/8"	1/2"	5/8"	3/4"	- P"	1 1/4"	1 1/2"	2"			
0.2	0.67	0.36	0.25	0.18	0.11	0.07	0.05	0.03			
0.3	1.00	0.54	0.37	0.27	0.16	0.11	0.08	0.05			
0.4	1.33	0.72	0.50	0.36	0.22	0.15	0.11	0.06			
0.5	1.67	0.91	0.62	0.45	0.27	0.18	0.13	0.08			
0.6	2.00	1.09	0.74	0.54	0.33	0.22	0.16	0.09			
0.7	2.33	1.27	0.87	0.64	0.38	0.26	0.18	0.11			
0.8	2.67	1.45	0.99	0.73	0.44	0.29	0.21	0.12			
0.9	3.00	1.63	1.12	0.82	0.49	0.33	0.24	0.14			
1.0	3.33	1.81	1.24	0.91	0.55	0.37	0.26	0.15			
LI	3.67	1.99	1.36	1.00	0.60	0.40	0.29	0.17			
1.2	4.00	2.17	1.49	1.09	0.66	0.44	0.32	0.18			
1.3	4.34	2.35	1.61	1.18	0.71	0.48	0.34	0.20			
1.4	4.67	2.53	1.74	1.27	0.76	0.51	0.37	0.22			
1.5	5.00	2.72	1.86	1.36	0.82	0.55	0.40	0.23			
1.6	5.34	2.90	1.98	1.45	0.87	0.59	0.42	0.25			
1.7	5.67	3.08	2.11	1.54	0.93	0.62	0.45	0.26			
1.8	6.00	3.26	2.23	1.63	0.98	0.66	0.47	0.28			
1.9	6.34	3.44	2.36	1.72	1.04	0.70	0.50	0.29			
2.0	6.67	3.62	2.48	1.81	1.09	0.73	0.53	0.31			
2.5	8.34	4.53	3.10	2.27	1.36	0.92	0.66	0.38			
3.0	10.00	5.43	3.72	2.72	1.64	1.10	0.79	0.46			
3.5	11.67	6.34	4.34	3.18	1.91	1.28	0.92	0.54			
4.0		7.24	4.96	3.63	2.18	1.47	1.05	0.62			
4.5		8.15	5.58	4.08	2.46	1.65	1.19	0.69			
5.0		9.05	6.20	4.54	2.73	1.84	1.32	0.77			
6.0		10.86	7.44	5.44	3.28	2.20	1.58	0.92			
7.0			8.68	6.35	3.82	2.57	1.84	1.08			
8.0			9.92	7.26	4.37	2.94	2.11	1.23			
9.0	L		11.16	8.17	4.91	3.30	2.37	1.39			
		Table	3.2 – FI	ow Velo	ocity (cor	ntinued)					
Flow Rate	Flow Rate ft/sec										
								2000			

110W Mate					i c c			
GPM	3/8"	1/2"	5/8"	3/4"	1"	1 1/4"	1 1/2"	2"
10.0	1			9.07	5.46	3.67	2.64	1.54
11.0				9.98	6.01	4.04	2.90	1.69
12.0	- J			10.89	6.55	4.40	3.16	1.85
13.0					7.10	4.77	3.43	2.00
14.0					7.64	5.14	3.69	2.16
15.0					8.19	5.51	3.95	2.31
	-	-	-	-		_		

Table 3.3 – Pressure Loss											
		6	0°F (16°C	C) Wate	r						
Flow Rate			Pressu	re Loss p	si/100 ft	of Pipe					
GPM	3/8"	I/2"	5/8"	3/4"	- 1"	1 1/4"	1 1/2"	2"			
0.2	0.427	0.099	0.040	0.019	0.006	0.002	0.001	0.0003			
0.3	0.880	0.204	0.083	0.039	0.012	0.005	0.002	0.001			
0.4	1.470	0.341	0.138	0.065	0.019	0.008	0.003	0.001			
0.5	2.189	0.508	0.205	0.097	0.029	0.011	0.005	0.001			
0.6	3.032	0.703	0.284	0.135	0.040	0.015	0.007	0.002			
0.7	3.993	0.926	0.374	0.177	0.053	0.020	0.009	0.003			
0.8	5.069	1.175	0.475	0.225	0.067	0.026	0.012	0.003			
0.9	6.258	1.450	0.586	0.278	0.082	0.032	0.014	0.004			
1.0	7.555	1.751	0.707	0.335	0.099	0.038	0.017	0.005			
I.I	8.960	2.076	0.839	0.397	0.118	0.046	0.021	0.006			
1.2	10.47	2.425	0.980	0.464	0.138	0.053	0.024	0.007			
1.3	12.08	2.799	1.131	0.535	0.159	0.061	0.028	0.008			
1.4	13.80	3.195	1.291	0.611	0.181	0.070	0.032	0.009			
1.5	15.61	3.615	1.460	0.691	0.205	0.079	0.036	0.010			
1.6	17.52	4.058	1.639	0.776	0.230	0.089	0.040	0.011			
1.7	19.53	4.523	1.827	0.865	0.256	0.099	0.045	0.012			
1.8	21.64	5.010	2.023	0.958	0.284	0.110	0.050	0.014			
1		Table	33-P	ressure	Loss (co	ntinued)					

and the second s		A REAL PROPERTY AND A REAL PROPERTY A REAL PROPERTY AND A REAL PRO
		Contraction American Advances of
	s - Praccure	ASS ICONTINUES

60°F (16°C) Water										
Flow Rate	Pressure Loss psi/100 ft of Pipe									
GPM	3/8"	1/2"	5/8"	3/4"	1"	1 1/4"	1 1/2"	2"		
1.9	23.84	5.519	2.229	1.055	0.313	0.121	0.055	0.015		
2.0	26.14	6.050	2.443	1.157	0.343	0.133	0.060	0.017		
2.5	39.00	9.024	3.643	1.724	0.511	0.197	0.089	0.025		
3.0	54.10	12.51	5.050	2.390	0.708	0.274	0.124	0.034		
3.5	71.36	16.50	6.658	3.150	0.933	0.360	0.163	0.045		
4.0		20.97	8.459	4.002	1.185	0.458	0.207	0.057		
4.5		25.90	10.45	4.943	1.463	0.565	0.256	0.071		
5.0		31.30	12.63	5.972	1.768	0.683	0.309	0.085		
6.0		43.44	17.52	8.284	2.451	0.946	0.428	0.118		
7.0			23.11	10.93	3.232	1.248	0.564	0.156		
8.0			29.38	13.89	4.108	1.585	0.717	0.198		
9.0			36.32	17.17	5.076	1.959	0.885	0.244		
10.0				20.75	6.134	2.367	1.070	0.295		
11.0				24.63	7.281	2.808	1.269	0.350		
12.0				28.81	8.514	3.284	1.484	0.409		
13.0					9.832	3.792	1.713	0.472		
14.0					11.24	4.332	1.957	0.539		
15.0					12.72	4.905	2.216	0.610		